



RESEARCH ARTICLE

EFFECT OF SELF-CURING AGENTS ON THE DIFFERENT PROPERTIES OF CEMENT AND MORTAR

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ABSTRACT

The effect of Polyethylene glycol (PEG) and Polyacrylamide (PAA) addition, on the properties of the ordinary cement and mortar, such as setting time, flow-ability, compressive, and tensile strength has been studied by adding 1,3,5,7wt% additive of PEG400 and (PEG/PAA) by weight of cement. Flexural strength has been determined using center point bending system. Bulk density and water absorption of resulting products was tested. The plain mortar specimens were prepared from Portland cement and the other specimens from the mixing of fly ash with cement together, which were cured by conventional method (water based-curing). Self-curing mortar was performed by adding Polyethylene glycol alone and the binary polymer blend (Polyethylene glycol/ polyacrylamide) with different weight ratios (1,3,5,7)% by weight of cement. Results indicate that the self-curing method under work has positive effect on the workability and strength of the mortar specimens. Mortar specimens cured by self-curing method exhibited higher efficiency in decreasing bulk density. It is found that the performance of self-curing is better than that of water-based curing. The data developed in this study indicates that the self-curing could be utilized in situations where curing with water is difficult. However, between the two investigated curing methods, self-curing mortar recorded better mechanical properties than the water-based curing mortar.

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INTRODUCTION

Concrete is a composite material that comprises of cement, aggregate, and water. It has been generally utilized for infrastructure construction, including pavements built on soil foundations and overlays paved on bridges to support vehicle loading. Under the effects of repeated vehicle loading, temperature cycling, material shrinkage, and chemical reaction, concrete structures may be experienced with cracking and interface debonding that shorten their service life and quality (Zengzhi, 2008). Polymer-modified cement materials have been utilized commercially in Portland cement mortars and concretes for more than 20 years, and yet they are still considered as relatively new in the construction industry. Concrete polymer composites are environment conscious and confirm to concerns of saving of natural resources, the longevity of infrastructures and environmental protection. Concrete has high compressive strength but relatively weak in tension and adhesion, and its porosity can lead to physical and chemical deterioration, while polymers are weaker in compression but have higher tensile strength, and provide good

adhesion to other materials as well as the resistance to physical (i.e., abrasion, erosion, impact) and chemical attack. Combinations of these two materials can exploit the useful properties of both composites with excellent strength and durability properties (Muthadhi, 2014). Polymer-modified cement are materials, which are made by polymeric binders that fractional replacement of hydraulic cement. Ordinary cement displays low flexural strength which differs with its chemical compositions and level of hydration and thus cement is never used in tension without the reinforcement. The addition of water-soluble polymers allows the formation of highly workable paste with very little water. The additive acts as lubricant facilitating close packing of different constituents which are then held tightly together causing higher strength and toughness observed in the modified cement products (Rai, 2005). Polymer alteration for cementitious material nowadays is utilized in rebuilding also repair industry and in particular situations, where high requests forwards adhesion, durability and climate capacity (Aggarwal, 2007). Curing of mortar is the maintain operation of the suitable moisture conditions to build up optimization cement hydration instantly after positioning. With inadequate water the hydration will not progress and the mortar producing may not possess the desired strength. The near surface region of mortar is particularly affected, failing to provide a protective barrier against ingress of harmful agents.

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However, even in mixes containing enough water, any loss of moisture from the mortar will diminish the initial W/C proportion and result in inadequate hydration of cement particularly with mixes having low W/C proportion, this results in extremely low quality of mortar (Venkateswarlu, 2015). Curing permits continuous hydration of cement and consequently continuous gain in the strength, once curing stops strength gain of the concrete also stops. Different variables for example wind velocity, relative humidity, atmospheric temperature, ratio of water/cement of the mixture and cement type (Junaid, 2015). Currently a large number of technicality are introduced with rapid improvement in the mortar technology. Self-curing technique is one of the techniques, used in less water resource places. The utilization of self-curing admixtures is extremely imperative from the viewpoint of water provision needed daily (Jagannadha, 2012).

The idea of self-curing agents is to diminish the water evaporation from concrete, and hence increment the capacity of water retention of the concrete compared to conventional concrete. These compounds will rise to the finished concrete surface and effectively seal the surface against evaporation. It was found that water soluble polymers can be used as self-curing agents in concrete. The utilization of self-curing admixtures is very important from the point of view that water resources are getting valuable every day (i.e., each 1 m³ of concrete requires about 3 m³ of water for construction most of which is for curing). The benefit of self-curing admixtures is more significant in desert areas where water is not adequately available (Siddharth, 2015). In the self-curing technique continuous evaporation of moisture takes place from an exposed surface due to the distinction in chemical potentials (free energy) between the vapors and fluid stages. Adding of polymers in the mixing mainly form hydrogen bonds with water particles and decrease the chemical potential of the atoms which thus diminishes the vapors pressure, thus lessening the rate of evaporation from the surface (Jagannadha, 2012 and Siddharth, 2015).

The findings of Rai and Singh's study,(2005) showed that the effect of polyacrylamide PAA addition on the properties of the ordinary cement and mortar. Setting time, heat of hydration, compressive and tensile strength were examined. The added polymeric phase is interspersed into cement causing decrease in water absorption and also its interaction with hydrating cement resulting furthermore bond formation leading to the increase in strength (Rai, 2005). The study of Suna and Xub, (2008) explained how polyacrylamide PAA modifies the physicochemical and mechanical properties of concrete. The microstructure of PAA modified concrete and the physicochemical reaction between PAA and concrete. PAA additionally fundamentally changes the microstructure at the aggregate–cement interfacial transition zone (Zengzhi, 2008). The study by El-Dieb's *et al.* (2012) indicated to the effect of utilizing water-soluble polymers (polyethylene glycol PEG and polyacrylamide PAA) as self-curing agents on the water retention, degree of hydration, water absorption, permeable pores and microstructural characteristics of Portland cement mixes with and without silica fume as replacement of cement. It is found that the hydration rate at 28 days of hardening for mixes containing 8% silica fume is higher with using the blend (PEG+PAA). Examination of the microstructural characteristics demonstrated a denser microstructure and a lower tendency for formation microcrack of self-cured mixes (Amr, 2012). Other study by Dahanayake *et al.* (2014) showed

that the self-curing concrete is one type of advanced concrete, which cures itself by retaining water by content of moisture in it. The utilization of polyethylene glycoladmixture in conventional concrete helps better hydration and hence the strength of concrete (Patel Manishkumar Dahanayake, 2014). At the same time, Sathanandham *et al.*, (2014) reported that the utilization of shrinkage reducing admixture polyethylene glycol PEG 4000 in concrete which helps in self-curing and helps in better hydration and hence strength, the effect of admixture (PEG 4000) on compressive strength, split tensile strength and modulus of rupture by varying the percentage of PEG by weight of cement from 0% to 2%. It was found that PEG 4000 could help in self-curing by giving strength on par with conventional curing. It is found that addition of 1% of PEG 4000 by weight of cement can be considered ideal for M20 grade concrete to obtain the maximum strength without compromising workability (Sathanandham, 2013). The research conclusions by Mousa *et al.*, (2014) illustrated that the mechanical properties of concrete containing self-curing agents, two materials were chosen as self-curing agents with various amounts, and the addition of silica fume was examined. The self-curing agents of pre-soaked lightweight aggregate (LECA) and polyethylene-glycol PEG (CH) were used. The result demonstrates that concrete utilized polyethyleneglycol as self-curing agent, achieved higher values of mechanical properties than the concrete with saturated LECA (Magda, 2015). Bashandy's study,(2016) reported that the self-cured concrete is a concrete type which can be cured without utilizing any external curing regimes. It can perform by few techniques, for example using lightweight aggregate or chemical agents (Bashandy, 2016).

Polymer Blends

A polymer is a material composed of macromolecules, built by covalently bonding at least 50 molecular mers or the constitutional repeating units. The mainchain may be composed of a series of subchains, identified by some chemical or physical characteristic. The main chain may also contain long or short side chains or branches, attached to it at the branch points. A little locale in a macromolecule from which at least four chains emanate constitutes a cross-linking point. A macromolecule that has just one cross-link is the star macromolecule. A macromolecule comprising of a few cross-linked chains, but having a limited molecular weight, is a micronetwork (Leszek, 2010). A polymer blend is a mixture of at least two polymers that have been mixed together to make another material with various physical properties, polymer blend is mixture of no less than two macromolecular substances, polymers or copolymers. Some blends are miscible in a certain useful range of composition and temperature, but immiscible in others. Most compatible blends are immiscible and can be made compatible only by a variety of compatibilization techniques (Lloyd Robeson, 2014). The modification of already existing polymers is more economically viable than the development of new monomers for the production of new types of polymers. High-value-added materials can be obtained either by new polymerization methods or by alloying or blending, and reinforcing existing polymer materials. Polymer modification processes based on simple mechanical mixtures of two or more polymers originated a new class of materials called polymer blends. A polymer blend, analogous to metal alloys, is the mixture of at least two different polymers to create a new type of material with different physical properties. The performance of polymer

blend depends on the properties of each polymer in the blend, their content, and morphology. The cost of the blend depends on the material, compounding method, and blend morphology, which can be tailored for a specific application. Most blends have been developed for the improvement of a specific property such as impact strength, or extending the performance of an engineering resin, improving the process ability or recycling facility, etc.

Polymer blends can be classified into the following categories:

- **Miscible Polymer Blends.** These are homogeneous blends with a single-phase structure. In this case, one glass transition temperature will be observed.
- **Immiscible Polymer Blends.** These blends have large size domains of dispersed phase and poor adhesion between them. If the blend is formed by two polymers, two glass transition temperatures will be observed.
- **Compatible Polymer Blends.** These are immiscible polymer blends that exhibit macroscopically uniform physical properties caused by sufficiently strong interface interactions between the polymer blend components.
- **Compatibilized Polymer Blends.** Immiscible blends in which the microstructure and physical properties can be stabilized by adding surface-active species called compatibilizers. These compatibilizers will influence various morphological processes, such as deformation, breakup, and coalescence of droplets (Enrique Saldívar-Guerra, 2016).

The main objective of this paper is to study how binary polymer blend (PEG/PAA) modifies mortar's engineering properties, such as compressive, flexural and tensile strength, bulk density of mortar as well as study the effect of weight ratio of the polymer blend (PEG/PAA) on all these properties of the prepared mortar.

Experimental Work

Materials and their Properties

Cement

Iraqi ordinary Portland cement produced by (AL-Christa) cement factory (type I) was used throughout this study. It was put away in a dry place (air-tight plastic containers) to lessen the effect of humidity and temperature. The chemical composition and physical properties of this cement are given in (Tables 1 and 2), respectively. Test results demonstrate that the adopted cement complies to the Iraqi specifications (IQS No.5/1984) (Iraqi standard Specification, 1984).

Fine Aggregate

The fine aggregate, natural sand was utilized all through this work of 4.75mm most extreme with grading limited zone II. (Table 3) reports the sieve analysis were made in the laboratory. Results indicate that the fine aggregate grading were within the requirements of the Iraqi specification (IQS No. 45/1988) (Iraqi Standard Specification, 1984).

Table 1. Chemical composition and main compounds of cement

Composition of Oxide	Abbreviation	Percentage by Weight	Limits of (IQS NO.5 /1984)
Lime	CaO	66.11	-
Silica	SiO ₂	21.93	-
Alumina	Al ₂ O ₃	4.98	-
Iron oxide	Fe ₂ O ₃	3.10	-
Sulphate	SO ₃	2.25	≤ 2.8 %
Magnesia	MgO	2.0	≤ 5 %
Loss on Ignition	L.O.I	2.39	≤ 4 %
Insoluble Residue	I.R.	1.29	≤ 1.5 %
Lime Saturation Factor	L.S.F.	0.93	0.66 – 1.02
Main Compounds (Bogue's equations)			
Name of Compound	Formula	Abbreviation	Percentages
Tricalcium silicate	3CaO.SiO ₂	C ₃ S	58.16
Dicalcium silicate	2CaO.SiO ₂	C ₂ S	19
Tricalcium aluminate	3CaO.Al ₂ O ₃	C ₃ A	7.95
Tetracalciumaluminoferrite	4CaO.Al ₂ O ₃ .Fe ₂ O ₃	C ₄ AF	9.43

*Chemical tests were made by the National Center for Construction Laboratories and Research (NCCLR)

Table 2. Physical properties of cement

Physical property	Test Results	Limits of Iraqi Specification No.5/1984
Specific surface area (Blaine method), m ² /kg	376	≥ 230
Setting time (viciat's method) Initial :by minutes	2.05	≥ 1 hr.
Final, by minutes	4.00	≤ 10.00 hrs.
Soundness (autoclave method) %	0.12	≤ 0.8%
Compressive strength (70.7mm cube) (N/mm ²) 3days	20	≥ 15
7days	25	≥ 23

*Physical tests were made by the National Center for Construction Laboratories and Research (NCCLR).

Table 3. Grading of fine aggregate used throughout this work

Sieve size(mm)	Cumulative passing %	Limits of Iraqi Specification No.45/1988, zone (2)
10	100	100
4.75	96.6	90 -100
2.36	92.4	60 -90
1.18	85.8	30 – 70
0.6	74.4	15 -34
0.3	40.3	5 -20
0.15	6.9	0 -10

Polyethylene Glycol

PEG 400H (OCH_2CH_2)_n OH is highly hydrophilic. PEG400 is soluble in water, acetone, alcohols and is somewhat soluble in hydrocarbons. Rely on molecular weight the extensive variety of the physicalproperty such as solubility, Hygroscopic, vapor pressure, freezing point and viscosityare variable, solubility increasing the molecular weight of PEG results in diminishing solubility in water and solvents.

Polyacrylamide

PAA is a water-soluble acrylate polymer formed from acylamide subunits. It is highly water-affiliated because of the amide ionogenin of its molecular chain, the NH₃ released through hydrolysis reacts with cations such as Ca²⁺ and Al³⁺ to modify the physical properties of concrete. PAA may exist in

three configurations: solvent colloid, latex, and dry powder. It can be mixed directly with cement, aggregate, and water to compose concrete without the need for additional equipment.

Table 4. Specifications of PEG400 according to the manufacturer

Average Molecular Weight	380-420 g/mole
Viscosity at 20°C	85-105 Cs
Weight per ml at 20°C	1.12g
Shape and appearance	Viscous Liquid
Color	Colourless

Anionic PAA is most suitable for inducing cement flocculation because its anions interact with Ca^{+2} ions produced by mortar hydration. PAA can improve the impermeability, penetration resistance, and workability of cement mortar, and the flexural and tensile strengths, toughness of cement and mortar (1). Polyacrylamide has CH_2 and NH_2 functional groups out of which NH_2 which on hydrolysis is likely to interact with cement phases forming products which remain dispersed uniformly in the rest of the materials modifying the physical and mechanical properties of the product. Thus increase in mechanical properties is not only because of the physical interaction between the cement and polymer producing a dense microstructure of very low porosity but also because of chemical interaction between the cement phases and the functional groups present in the additive (3).

Table 5. Specifications of PAA according to the manufacturer

Average Molecular Weight	5000000 g/mole
Stability	Stable
Water Solubility	Soluble
Density at 25°C	1.189 g/ml
Shape and appearance	Powder
Colour	White

Fly Ash

Fly ash is fine and glassy powder that is recuperated as an aftereffect of coal burning during creation of electricity from ISKENment-Turkey power station. It is viewed as coal ignition waste. Composition of Fly ash relies on upon source. Fly ash particles are mostly spherical in shape and range in size from 0.5 μm to 100 μm . Two fundamental types of fly ashes: one Class F fly ash and Class C fly ash. Class F fly ash has been explored and it contains not exactly than 20% CaO (ASTM C 618, 2005) (19).

Table 6. Chemical Composition of Fly ash

Materials	SiO ₂ %	Al ₂ O ₃ %	CaO%	SO ₃ %
Fly ash	57.36	19.17	1	0.07

Strength Activity Index for Fly Ash

The strength activity index for Fly Ash is conducted according to the ASTM C311-05.

Mix Procedure

Distinctive mixes were utilized to examine the effect of PEG/PAA on the compressive, tensile, flexural strength and bulk density of mortar. (Table 7) gives the specifics of the mix proportions. The reference mix M* had weight of 1 cement to 2 sand and mix M had weight of 1 cement to 2.5 sand with 5%

fly ash of weight of cement and did not include PEG/PAA. Mixes M1, M3, M5 and M7, the PEG/PAA mortar of 1, 3, 5 and 7 wt.% respectively.

Table 7. Mix proportions

Mix type	Cement g	Sand g	C/S ratio	W/C ratio	G%	Fly ash g	PB/C ratio
M*	500	1000	1:2.5	0.35	3.5	-	-
M	475	1000	1:2.5	0.35	3.5	25	-
M1	475	1000	1:2.5	0.3	3	25	1
M3	475	1000	1:2.5	0.3	3	25	3
M5	475	1000	1:2.5	0.3	3	25	5
M7	475	1000	1:2.5	0.3	3	25	7

Before molding, the molds were oiled carefully to be prepared for casting fresh mortar. The mortar was cast in layers (3 layers) for all specimens; every layer was compacted by a rod then all specimens were wet-cured by covering the completed surface and molds with polyethylene sheet. After one day, the molds were opened and the specimens were cured in water for a period of 7, 28 and 90 days except PEG/PAA mortar which was cured in air for the same duration. High performance Superplasticizer admixture (Glenium 54) has appropriate consistency with low water to binder (W/B) ratio and tap water is utilized as a part of the test work for both mixing and curing purposes of conventional, self-curing mortar.

Testing of Fresh Mortar

Setting time: This test was specified according to the ASTMC191-03(20). This procedure is utilized to determine initial setting and final setting time of cement paste by utilizing Vicat needle.

Flow Test : This test gives an allusion of the consistence of mortar and its inclination to isolation by measuring the spread of a pile of mortar undergo to jolting. It is concerning isolation that the flow test is of greatest value, yet it additionally gives a good estimation of stiff, rich, and rather cohesive mixes .The test was covered by ASTM standard C1437 – 15 (21).

Testing of Hardened Mortar

Compressive Strength: The compressive strength test was specified according to B.S.1881, part 16(22). This test was made on 50 mm cubes utilizing ancompression testing machine (ELE) with a capacity of 2000kN, a vibrating machine was used for uniform packing. Samples were kept in the mould in 90% relative humidity at $25\pm 2^\circ\text{C}$ for the first 24 h and then demoulded and kept in chamber at the same humidity and temperature for 7, 28 and 90 days for curing at $27\pm 2^\circ\text{C}$. Each compressive strength value was taken as the average of three samples. The compressive strength of the specimen was calculated by dividing the maximum load carried by the specimen during the test by the average cross-sectional area of the specimen.

Tensile Strength

A mortar sample is put with its horizontal axis between platens of tensile testing machine (ELE) with a capacity of 10kN.The tensile strength test was done according to BS 6319-7: 1985specification [23]. The mortar was prepared using 1:2 cement-sand mix (by mass) and water (w/c = 0.3) with additive. Briquettes were also kept in 90% relative humidity at

$27\pm2^\circ\text{C}$ for the first 24h and then demoulded and cured under similar conditions in the same humidity chamber for 7, 28 and 90 days. Each tensile strength value was taken to be an average of three samples. Form of dumb-bell shaped briquette test specimens were utilized and load was connected constantly up to failure.

Flexural Strength

The flexural strength test was measured by using prism specimens with dimensions of 160 mm length, 40 mm width and 40 mm thickness. The specimen was subjected to simply support over the length of the prism on perpendicular direction of cast and the load was applied in the center of the prism. The test was obtained by 10kN Flexural/Tensile testing machine of ELE International company. This machine is given the maximum load of flexural process in kN and the flexural strength was calculated according to ASTM C293-02 (24) by the equation:

$$Fr=3PL/2bd^2 \dots\dots\dots (1)$$

Where

Fr: Modulus of rupture (flexural strength MPa)

P: maximum load (N)

L: length of the span(mm)

b: width of the specimen (mm), and

d: thickness of the specimen (mm)

Center point load test was carried out according to ASTM C293-02 using ELE (10)kN capacity machine. Average modulus of rupture of three prisms was obtained for each testing age (7,28 and 90) days.

Bulk Density

The bulk density test was specified by B.S 1015, Part 10(25). Three test samples of standard shape are set up from the fresh mortar to be tested and cured. The hardened test samples are dried to a constant mass at a temperature of 70°C , the dry mass is recorded and the volume of the test specimens is determined. The bulk density of each test specimen is computed by divided the mass on volume of specimen.

Water Absorption

The Water absorption test was specified by ASTM (27). Water absorption measurements were carried out on the cubic specimens with specific cross-sectional. Mortar specimens was prepared adopting to the same mixing condition as for strength specimens, after demoulding, specimens were immersed into water within 25°C . The absorbed water was calculated as the difference between saturated and dry masses of specimens. The test was carried out by weighing the specimens before the test. All tests were performed at 7, 28 and 90 days for all mixes of mortar. These properties are particularly important in concrete, as well as being important for durability. It can be used to predict mortar durability to resist corrosion. This test was determined according to the ASTM C642-97 (27). The water absorption is determined by dividing the weight difference of specimen on its dry weight.

$$A= [(Ws-Wd)/Wd] \times 100 \dots\dots\dots (2)$$

A=absorption value (%).

Ws=saturated or wet weight of specimen after immersion it into water for certain time, (g).

Wd= dry weight of specimen in air, (g)

RESULTS AND DISCUSSION

Setting Time

The setting time of cement containing 1,3,5,7 wt% of PEG400 and polymer blend (PEG/PAA) are given in (Table 8). The value of initial setting time and final setting time of cement paste was observed to be 72 and 110 min, respectively. It is evident from the Table that when PEG400 and (PEG/PAA) is mixed with cement it changes the setting time. It was found to act as a retarder and has prolonged the initial setting time from 77 to 84 min with 1,3,5,7 wt % addition of PEG 400 in cement. Final setting time was also prolonged from 123 to 155 min for similar percentages of 1,3,5,7 wt % added in cement, and the initial setting time from 88 to 97 min with 1,3,5,7 wt % addition of (PEG/PAA) in cement. Final setting time was also prolonged from 188 to 227 min for similar percentages of 1,3,5,7 wt % added in cement. It is the characteristic property of the functional group in the organic compound, its nature, chain length etc, which effect the cementitious properties of cement in which it is mixed, it has been demonstrated that it may be essentially due to retarding of the hydration of $3\text{CaO} \cdot \text{SiO}_2$ through the chemisorption of organic molecule on to $\text{Ca}(\text{OH})_2$ nuclei. The hydroxyl group being polar and hygroscopic in nature, thus, diminishes the amount of water available for the hydration of silicate. It appears that the retardation procedure in the presence of PEG400 and (PEG/PAA) because of the chemical interaction between hydrated cement phases (C_3S , C_2S and C_3A) and polar functional groups of organic polymers to yield amorphous materials, which are scattered between the crystalline mass of cement paste (3).

Table 8. Setting time of all mixes

Mix type	Setting Time/min	
	Initial Time	Final Time
R	72	110
F	75	116
E1	77	123
E3	78	125
E5	80	150
E7	84	155
B1	88	188
B3	89	198
B5	92	213
B7	97	227

Flow Test: The effect of polymer addition on W/C ratio required to maintain the desired flow (105–115 mm). The needed quantity of water decreases with the addition of both polymers. The fluidity and water-reducing effect increases with increasing PEG400 and (PEG/PAA) percentage. This might affect starting with the water-absorption effect of PEG400 and (PEG/PAA), and also those lubrication effects of the formed latex around cement particles will lessen the W/C proportion from 0.35 to 0.3, and with addition of fly ash, it is found that the presence of very fine fractions has positive effect on the workability of the mix (26).

Compressive Strength: The test results of compressive strength, (it may describe material brittleness) at a curing age of 7, 28 and 90 days are detailed in (Table 9). The PEG400 and (PEG/ PAA) modified mortar displays higher compressive strength, which concurs with other investigation on the PEG400 and (PEG/ PAA) modified cement mortar, and lower brittleness than reference mortar which may be attributed to the continuation of the hydration procedure, which leads to,

lower voids and pores, and greater bond force between the cement paste and aggregates (12). However, it demonstrates that the compressive strength decreases to some extent. Meanwhile, it diminishes with increasing PEG400 and (PEG/PAA)/C proportion. Therefore, PEG400 and (PEG/PAA) modified mortar might viably enhance the performances of these infrastructures. The chemical interaction between cement and polymer functional group also contributes to the improvement of mechanical properties. The compressive strength of fly ash mortar at 7, 28 and 90 days were observed to be 20.6, 23.1 and 24.2 MPa as shown in (Table 9) and the graphical representation which is appeared in (Figure 1) In the mixes of PEG400 and (PEG/PAA) mortar, 3wt% additive content at 7 days has given maximum compressive strength 23.2 MPa, at 28 days, 25.9 MPa and at 90 days, 27.6 MPa, and in the mixes of (PEG/PAA) mortar, 3wt% additive content at 7 days has given maximum compressive strength 20.3 MPa, at 28 days, 21.7 MPa and at 90 days, 25.1 MPa. The effect of strength relies on upon the nature and amount of additive and W/C ratio. The organic set retarders increase the strength of mortar at late curing periods (3). The partial replacing of cement with fly ash caused increase in compressive strength of PEG400 and (PEG/PAA) modified mortars at the all ages of curing (26).

Table 9. Compressive strength results of polymer blend (PEG/PAA) modified mortar specimens

Mix type	Compressive strength (MPa)		
	7 day	28 day	90 day
R	19.3	22.2	23.6
F	20.6	23.1	24.2
E1	22.6	25.7	27.4
E3	23.2	25.9	27.6
E5	20.8	21.4	24.6
E7	18.4	19.6	20.3
B1	19.8	22.8	25.9
B3	20.3	21.7	25.1
B5	16.7	17.5	22.4
B7	16.1	16.8	19.8

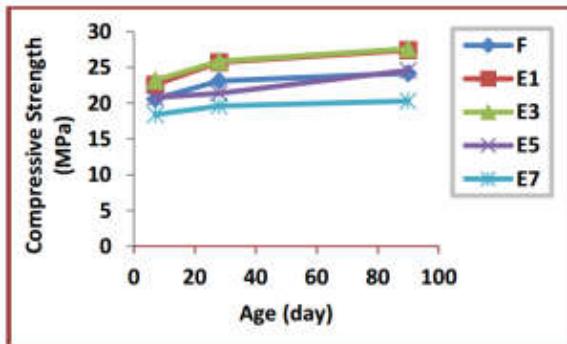


Figure 1. Compressive strength results of (PEG400) modified mortar specimens at 7, 28 and 90 days

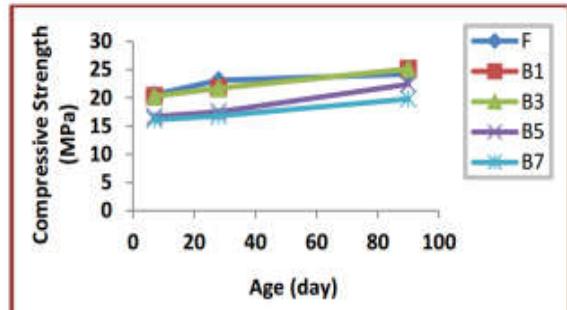


Figure 2. Compressive strength results of polymer blend (PEG/PAA) modified mortar specimens at 7, 28 and 90 days

The PEG400 and polymer blend (PEG/PAA) provided optimum results compared to other curing methods. There was a slight lessening in the compressive strength with the addition of self-curing agent at 5,7wt% of PEG400 and (PEG/PAA) (5).

Tensile Strength

Test results of mortar containing polymer blend (PEG/PAA) with various proportions are represented in (Table 10) and the graphical representation is appeared in (Figure 3,4) Results indicated higher strength of mortar with PEG400 and (PEG/PAA) relative to reference mortar. After 7,28 and 90 days, the strength of mortar with 1,3,5,7 wt% increase compared to reference mortar, the incorporation of self-curing agents into mortar mixtures provides internal curing for the mortar and thus permitting continuous hydration, which results in an improvement in the tensile strength of the mortar (12), these results are tabulated below.

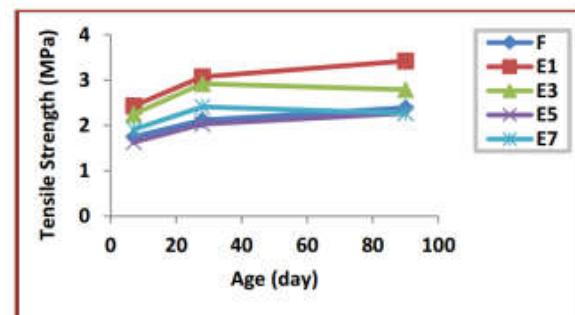


Figure 3. Tensile strength results of polymer blend (PEG/PAA) modified mortar specimens at 7, 28 and 90 days

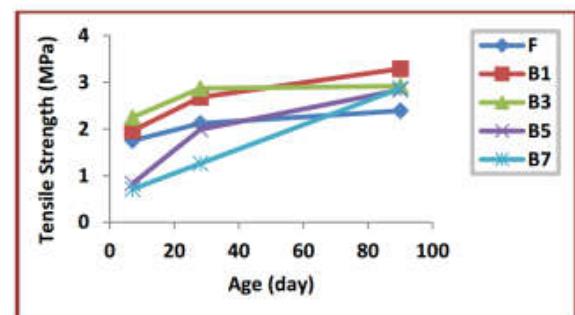


Figure 4. Tensile strength results of (PEG400) modified mortar specimens at 7, 28 and 90 days

Table 10. Tensile strength values of polymer blend (PEG/PAA) modified mortar specimens

Mix type	Tensile strength (MPa)		
	7 day	28 day	90 day
R	1.37	2.07	2.39
F	1.75	2.12	2.65
E1	2.43	3.07	3.42
E3	2.25	2.92	2.79
E5	1.63	2.03	2.27
E7	1.91	2.41	2.68
B1	1.96	2.68	3.29
B3	2.25	2.87	2.92
B5	0.83	1.99	2.84
B7	0.71	1.26	2.87

Flexural Strength

The results of the flexural strength are represented in (Table 11) and the graphical representations are shown in (Figures

5&6) The flexural strength was found to increase up to 5, 7 wt% of (PEG/PAA) modified mortar. The flexural strength values acquired were 4.38, 6.39, 11.08 MPa with 3wt% of PEG400 after curing for 7, 28 and 90 days, respectively, and the flexural strength values of (PEG/PAA) were 6.05, 6.88, 10.02 MPa with 1wt%. These values increase with increasing percentage of PEG400 and (PEG/PAA), at the lower W/C proportion of 0.3. Ordinary cement displays low flexural strength which varies with its chemical compositions and level of hydration and therefore cement is never utilized in tension without the reinforcement. The addition of water-soluble polymers allows the formation of highly workable paste with very little water. The additive acts as lubricant facilitating close packing of different constituents which are then held tightly together causing higher strength, addition of polymer blend (PEG/PAA) are interspersed and react with each other at room temperature to make a material with high flexural strength, which is free from defects (3).

Table 11. Flexural strength values of polymer blend (PEG/PAA) modified mortar specimens

Mix type	Flexural strength (MPa)		
	7 day	28 day	90day
R	3.05	3.4	5.11
F	3.22	3.9	5.31
E1	4.09	7.34	10.44
E3	4.38	6.39	11.08
E5	4.3	5.67	10.57
E7	4.89	5.38	8.25
B1	6.05	6.88	10.02
B3	5.10	5.49	9.20
B5	4.56	4.41	8.68
B7	4.65	5.91	8.27

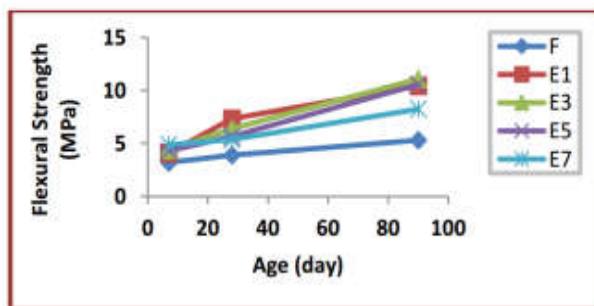


Figure 5. Flexural strength results of (PEG400) modified mortar specimens at 7, 28 and 90 days

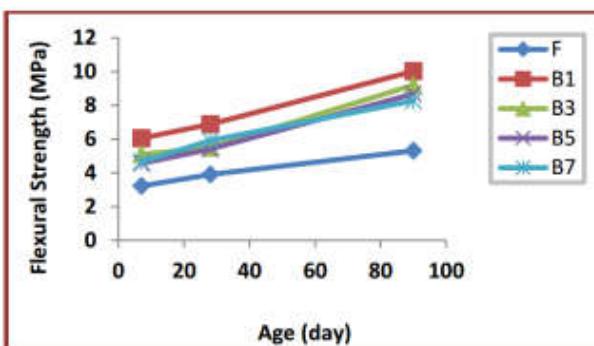


Figure 6. Flexural strength results of polymer blend (PEG/PAA) modified mortar specimens at 7, 28 and 90 days

Bulk Density

The influence of polymer blend (PEG/PAA) on bulk density of polymer-modified hardened mortar was studied. (Table12)

illustrates that the bulk density of all mortar mixes (self-curing and reference mortars) diminishes gradually with time under air curing, due to water dissipation from mortar. The varieties of bulk density due to changes in C/P proportion are appeared in (Figures 7, 8) at different self-curing periods. As indicated by this figure, it can be concluded that any increments in C/P proportion in the given range result in a significant decrease in bulk density. Such a positive effect of PEG 400 and (PEG/PAA)on hardened mortar can be absolutely credited to the lubricating effect of which improve both dispersion and close packing of cement molecules which are then held closely with each other by the binding properties of both hydration products of cement phases and the polymer matrix created. The presence of fly ash and self-curing agents in mortar caused an extra diminishment in bulk density relative to conventional mortar during the experiment to confirm that a better water retention happened. The mortar containing 5% of fly ash and 7wt% of PEG400 and (PEG/PAA) showed better performance compared to the reference mortar.

Table 12. Bulk density values of polymer blend (PEG/PAA) modified mortar specimens

Mix type	Bulk Density (g/cm ³)		
	7 day	28 day	90 day
R	2.63	2.32	2.15
F	2.52	2.45	2.37
E1	2.11	2.12	2.04
E3	2.22	2.24	2.14
E5	2.17	2.13	2.12
E7	2.16	2.07	2.01
B1	2.17	2.14	2.11
B3	2.14	2.12	2.05
B5	2.12	2.1	2.03
B7	2.07	2.05	2

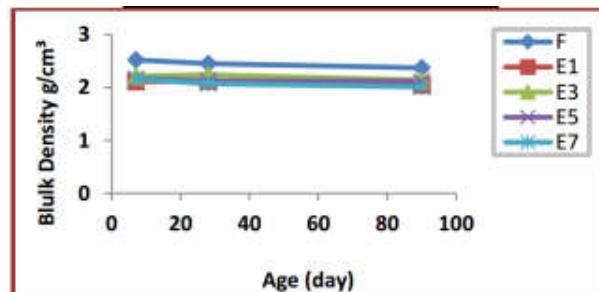


Figure 7. Bulk density results of PEG400 polymer modified mortar specimens at 7, 28 and 90 days

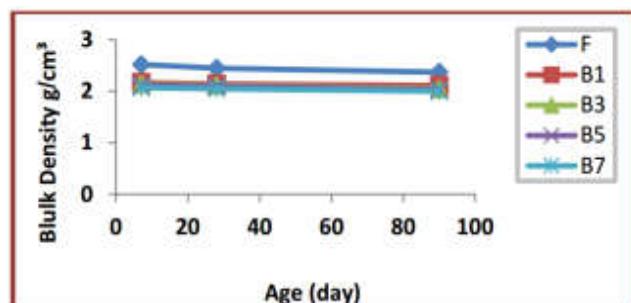


Figure 8. Bulk density results of PEG/PAA polymer modified mortar specimens at 7, 28 and 90 days

Figure 9 demonstrates the details of water absorption capacity of conventional concrete without self-curing compounds and with self-curing compounds. It is apparent from the results that

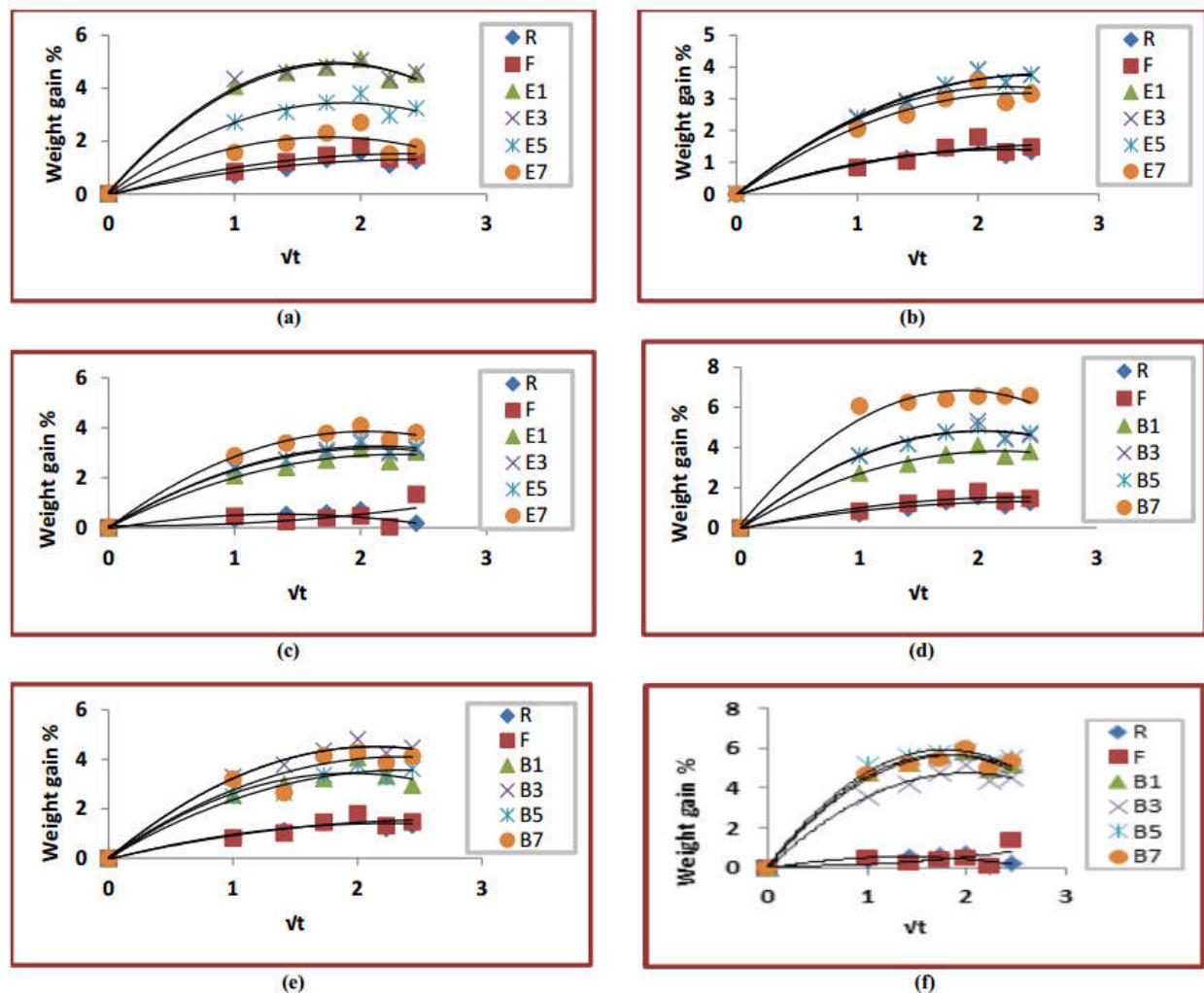


Figure 9. (a),(b),(c),(d),(e),(f) water absorption results of PEG400 and (PEG/PAA) polymer modified mortar specimens at 7, 28 and 90 days respectively

there is increase in the water retention capacity with the addition of self-curing compounds due to increase in the moisture content that is provided by the hydrophilic compounds. It can also be said that self-curing is giving optimum results compared to other curing conditions. The weight gain of the specimens were calculated and plotted against the in square root of time in days as appeared in (Figure 9) From this figure it is observed that weight gain increased with the addition of self-curing compounds when compared with water cured specimens (5).

Conclusion

The addition of PEG400 and (PEG/PAA), alters the physical and mechanical properties of cement mortar. The studies demonstrate that polymer-modified mortar possesses higher strength compared to reference mortar. Mortar with 1 and 3 wt% of PEG400 and (PEG/PAA) dosage gives higher compressive strength, as compared to conventionally cured mortar. This is because of reduction in porosity, with increment in rate of added substance. The organic polymer, interspersed in the hydrated cement may lead to the formation of crosslinks among the grains solidified in originally free space. By the use of PEG400, and (PEG/PAA) it is observed that the workability of mortar also increases, and mortar becomes flowable. Up to certain dosage, of PEG400 and (PEG/PAA) we can save water which is required for external

curing. It has been observed during testing; internally cured mortar PEG400 and (PEG/PAA) demonstrates lesser cracks than the mortar. Addition of PEG400 and (PEG/PAA) effectively enhances its tensile and flexural strength. However, the compressive strength decreases to some extent. Hence, PEG400 and (PEG/PAA) modifier can be a good candidate for infrastructure utilizes particularly those subjected to the flexural stress and interface shear stress, such as bridge overlays and pavements.

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