



RESEARCH ARTICLE

EVALUATION OF THE STRESS PATTERNS ON THE BONE AROUND AN IMPLANT USING VERTICAL AND ANGULATED ABUTMENTS: A FINITE ELEMENT ANALYSIS STUDY

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ABSTRACT

**Background:** Dental implants offer several benefits over conventional tooth replacements. Angulated abutments or a combination of angulated and straight abutments were used to support prostheses. Implant placement relates to emergence profile of the implant prosthesis and use of preangulated abutments to fulfill esthetic and functional objectives in selected cases.

**Aim and Objective:** The aim of the study was to evaluate stress patterns on the bone around an implant of vertical and angulated abutments using finite element analysis. The objective was to evaluate and compare the Von misesstress (overall stress) distribution of vertical ( $0^{\circ}$ ) and angulated ( $10^{\circ}$ ,  $20^{\circ}$  &  $30^{\circ}$ ) abutments in D2 and D3 types of density of bone.

**Materials and Method:** This study was conducted using finite element method. Two models were generated to simulate the D<sub>2</sub> and D<sub>3</sub> density bone using the digitized data computed from the computer tomography scans. Four groups of models with  $0^{\circ}$ ,  $10^{\circ}$ ,  $20^{\circ}$  and  $30^{\circ}$  abutments were analysed in ANSYS software. Axial loads of 178N was applied on the cingulum area of all the models.

**Results:** The results showed an increased magnitude of stresses of approximately 4.4 folds was observed at overall bone implant interface as angulations of abutments increased from  $0^{\circ}$  to  $30^{\circ}$  under axial loading in D2 and D3 density types of bone.

**Conclusion:** This concludes that Von Mises stresses were higher in  $30^{\circ}$  angulated abutment and increases from  $0^{\circ}$ ,  $10^{\circ}$ ,  $20^{\circ}$  &  $30^{\circ}$  on axial loading of 178N. However there was no significant differences was observed in magnitude of stresses in both D2 and D3 types of bone.

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INTRODUCTION

The goal of modern dentistry is to return patients to oral health in a predictable fashion. The partial and completely edentulous patients may unable to recover normal function, esthetics, comfort or speech with traditional removable prosthesis. Compared with traditional methods of tooth replacement, the implant prosthesis offers increased longevity, improved function, bone preservation and better psychological results (Carl.E.Misch,1999). A critical determinant for placement of an implant is the height and width of bone available in an edentulous sites. The clinician also needs to evaluate the angulation of the ridge, bony undercuts, shape of the arch, maxillomandibular relationships, position of mandibular canal and proximity of paranasal sinuses are considered before placing the implants. Ideally, implants should be placed parallel to each other and to adjacent teeth and be aligned vertically with axial forces. However, achieving this may not be possible owing to deficiencies in the ridge's anatomy.

To compensate for ridge topography that is less than ideal, the clinician can follow one of several scenarios to enhance placement of implants: augment the ridge, change the intended location of an implant by sinus elevation and nerve repositioning or insert an implant with an angled trajectory (John Cavallaro, 2011). The use of angulated abutments may provide a variety of advantages: facilitating placement of an implant with greater dimensions in width and height, avoiding guided bone regeneration (GBR) procedures, reduced treatment time, fees and aid the clinician in avoiding damage to anatomical structures when placing the implants. The use of angled abutments facilitates paralleling the nonaligned implants, thereby making prosthesis fabrication easier. The angulation of these abutments varies from  $15^{\circ}$  to  $35^{\circ}$  (Krishna Prasad, 2013). Clinical comparative studies of implant with straight abutments and angulated abutments showed that the bone loss or survival of angled abutment was not significantly different from straight abutment, however the strain gauge measurements and photo elastic models of Brosh et al and finite element analysis of Canay et al. revealed that angled abutment were subjected to higher stress values around the cervical region than those observed for straight abutment

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(Arun Kumar *et al.*, 2013). Angled abutments decrease the stress and promote better stress distribution on bone surrounding the single-unit dental implants. (Tian *et al.*, 2012) However, increased stresses on implants and bone have been associated with use of angled abutments. A finite element analysis was chosen for this study as it is useful tool in estimating stress distribution in the contact area of the implant with the bone.

## MATERIAL AND METHODS

As the finite element method requires a huge amount of computation, its application should be supported by advanced computer technology. The Von mises stresses on axial loading of implants along with straight and angulated abutments were calculated using three dimensional finite element models created on a workstation computer with following configurations

### Hardware

Intel(R) Core(TM) i3-3120M CPU Processor with a speed of 2.50 GHz 4 GB Ram.

### Software

ANSYS (R 14.5 Version), ANSYS corporation US.

### Application of finite element analysis

#### Maxillary bone

A three dimensional finite element solid model of the premaxilla was constructed based on CT data. It has been observed in numerous investigations that to assess stress distribution around dental implants, it is not necessary to build a finite element model of the entire maxillary arch, because of its complicated and individually different geometry. In this study the maxillary bone was not completely modeled, a part of the section of the maxilla in anterior esthetic zone involving D2 and D3 density was generated.

#### Finite element models

Two mathematical models were developed to simulate the D<sub>2</sub> and D<sub>3</sub> density bone using the digitized data computed from the computer tomography scans. The isotropic cortical bone thickness was 1.0 mm for D<sub>2</sub> and 0.5 mm for D<sub>3</sub> on the facial, lingual and occlusal aspects of the bone. The cancellous bone had a density approximately 17% that of cortical bone around an implant in both the models of model-1 and model-2 of maxillary bone of D2 type and maxillary bone of D3 type as shown in Figures 1a and 1b.

#### Implant model construction

The implant fixture model generated for the study was 4.2 × 13 mm. The simulated implant was a self-threaded, single piece, cylindrical fixture, with commercially pure titanium properties. Cementable abutments of angulations (0°, 10°, 20° and 30°) were used and analysed using Finite Element Analysis ANSYS software. Models were meshed with a four node tetrahedron elements as shown in Figures 2a, 2b, 2c and 2d. Depending on the implant size the number of elements and nodes in each group of model was shown in Table-1.

**Table 1. No. of elements and nodes**

	Number of elements	Number of Nodes
Straight	100442	21191
10deg	100565	21201
20deg	100669	21248
30dege	100594	21216

### Prosthesis model construction

Prosthesis superstructure of angulated abutments were modeled based on the original patient's clinical crown design from the CT dataset. Four different abutment angulations respectively 0°, 10°, 20°, 30° were used. The design and geometry of the model were assumed to be symmetric at 1.5 to 3.4 mm in thickness, 12.0 to 14.1 mm in width, and 15.0 to 17.3 mm in height. The prosthesis and its framework were modeled as one piece and assumed to be made with similar properties of titanium alloy for the analysis. After modeling the components were meshed using the software. All materials used in the models were considered to be isotropic, homogenous, static and linearly elastic. Axial loads of 178N will be applied on the cingulum area of all the models as shown in Figure 3. The loading was based on the average axial loading observed in the natural dentition (Hellsing, 1980)

### Interface conditions

To simulate ideal osseointegration the implants along their entire interface, were rigidly anchored in the bone model. The same type of contact was provided at all material interfaces as shown in Table-2 and Table-3. The friction coefficient,  $\mu$ , for all contacting surfaces was set at 0.3, to simulate an immediate loading condition (Jian-Ping Geng *et al.*, 2001)

### Properties of the members

**Table 2. D2 Bone Properties**

Details	Young's Modulus(Mpa)	Poison's ratio
Cortical Bone	13700	0.3
Cancellous Bone	1370	0.3
Implant(Titanium)	110000	0.35

**Table 3. D3 Bone Properties**

Details	Young's Modulus(Mpa)	Poison's ratio
Bone(Cortical & Cancellous)	10600	0.3
Implant(Titanium)	110000	0.35

### Methodology

- A series of CT image datasets of premaxilla model, implant models and prosthesis models were taken and meshed for the analysis.
- The conventional implant was virtually placed in the anterior region of the maxilla adjacent to the lateral incisor. All models were converted into four nodes of the tetrahedral element type in finite element analysis ANSYS software. The total number of elements for the D2 model was 3,02,380 tetrahedral elements while the D3 model had a total of 3,83,482 tetrahedral elements.
- The friction coefficient,  $\mu$ , for all contacting surfaces was set at 0.3 to simulate an immediate loading condition. Axial loads of 178 N will be applied on the cingulum area of all the models and Von Mises

stresses occurring for angulated abutments (0°, 10°, 20°, 30°) was interpreted and to compare the stress distribution on the bone around an implant in D2 and D3 types of density of bone.

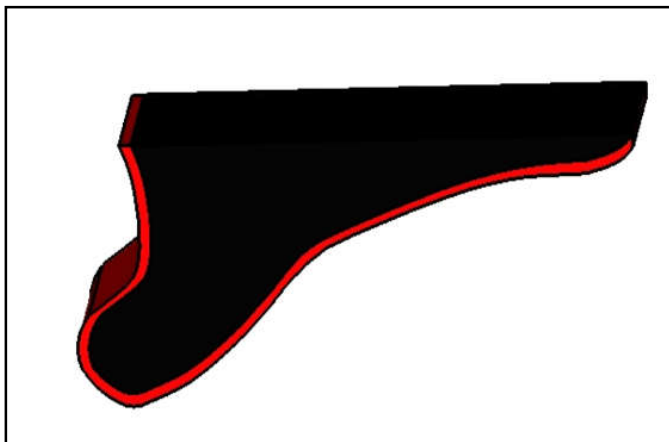
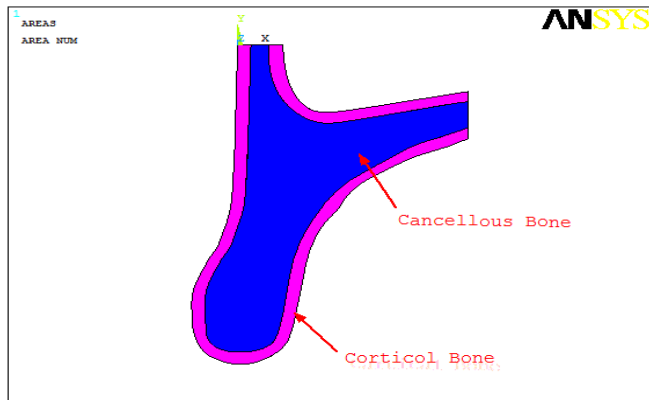


Fig. 1a&1b. Maxillary bone of D2 density and D3 density

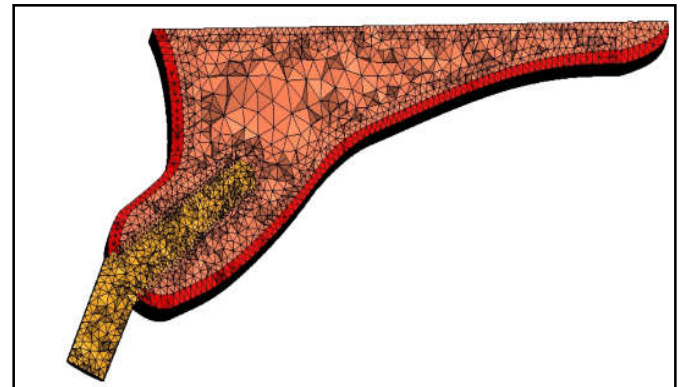
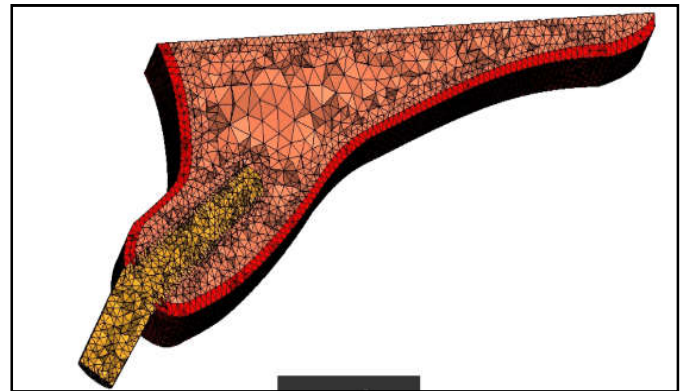


Fig. 2c&2d. 20° and 30° abutment model with elements, nodes

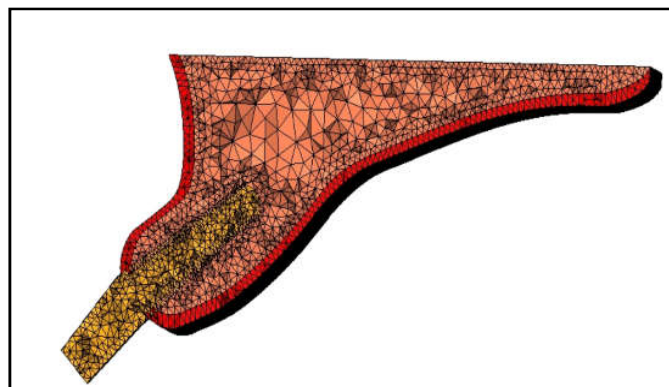
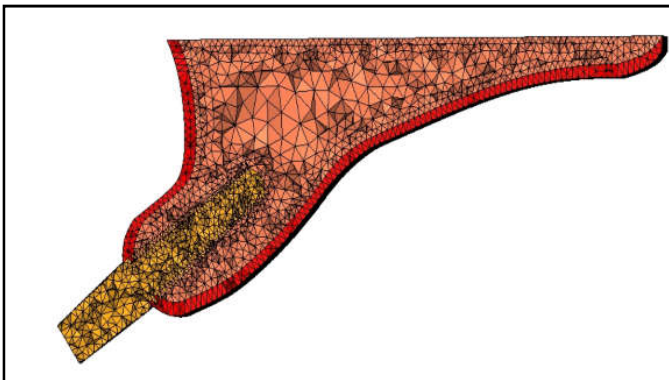


Fig. 2a&2b. Straight and 10° abutment model with elements, nodes

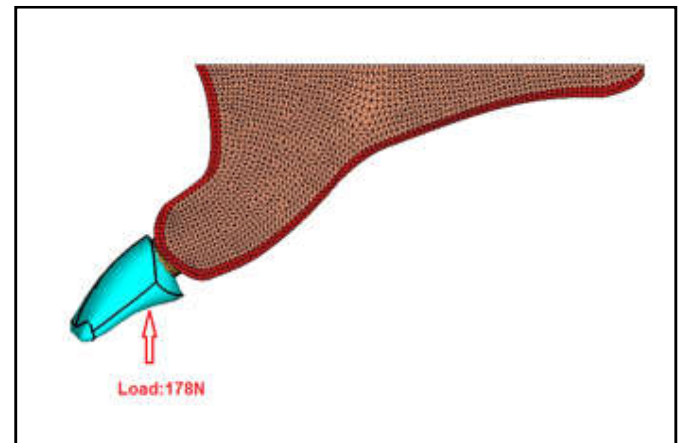
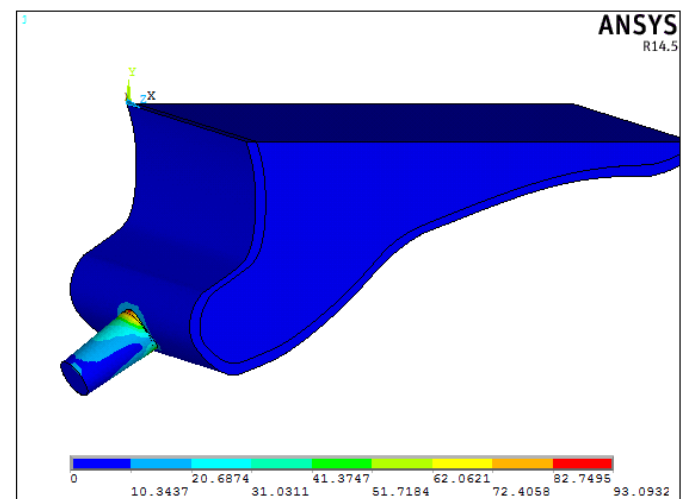


Fig. 3. Loading of prosthesis model



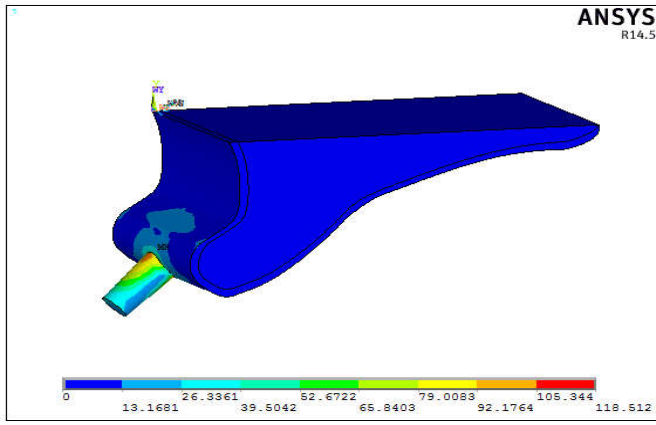


Fig. 4a&4b. Overall stress of 0° and 10° abutment in D2 bone

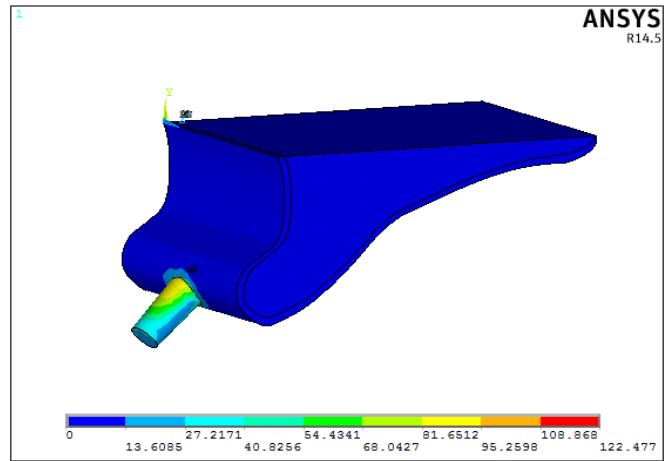


Fig. 5a&5b. Overall stress of 0° and 10° abutment in D3 bone

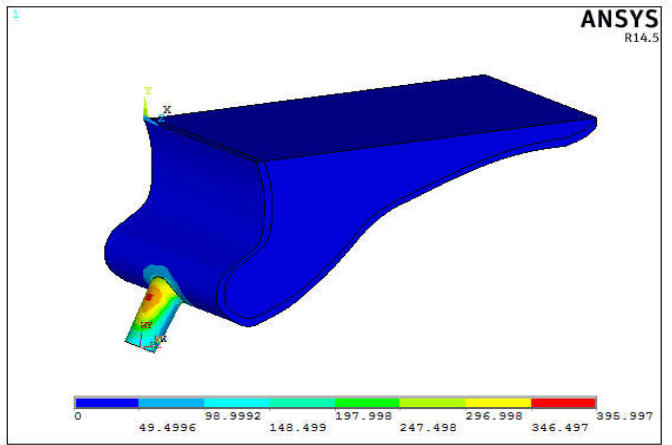
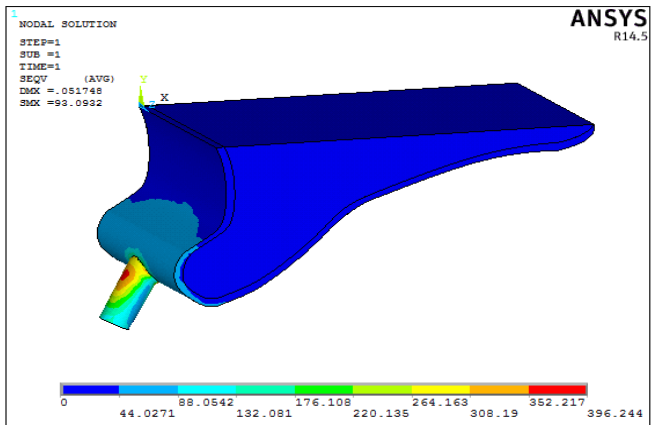
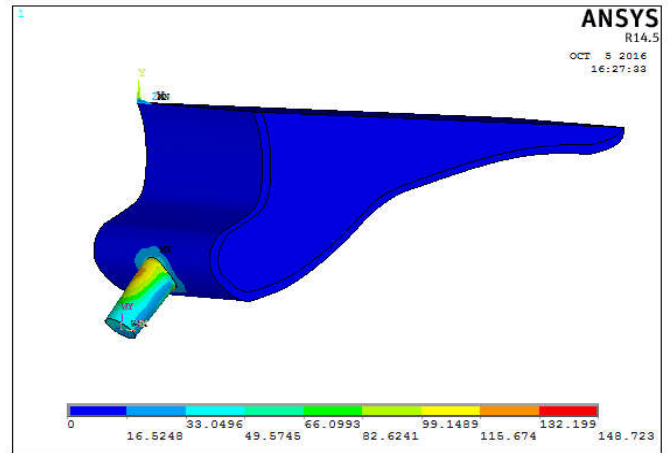
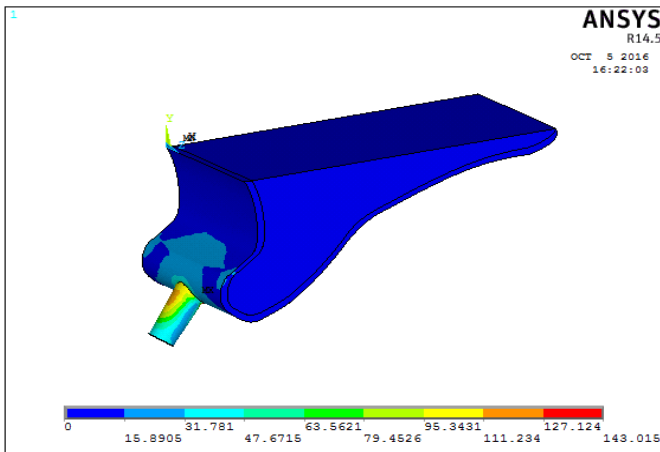


Fig. 4c&4d. Overall stress of 20° and 30° abutment in D2 bone

Fig. 5c&5d. Overall stress of 20° and 30° abutment in D3 bone

Table 1. Comparison of Magnitude of stresses (Mpa) recorded at different angulations of angulated abutments under axial loading of 178N in D2 density bone

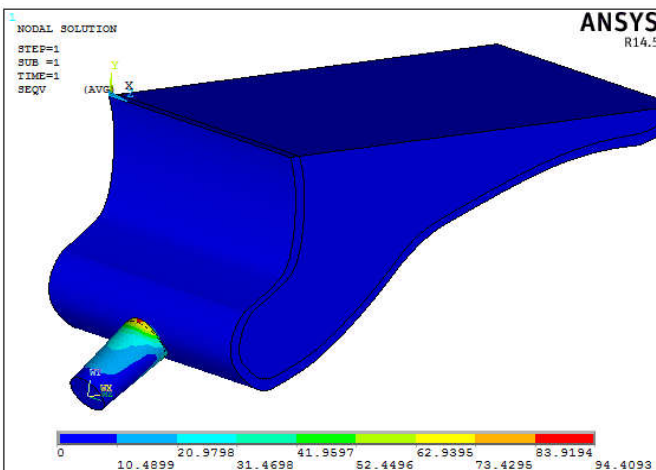
	Zero	10deg	20deg	30deg
Overall stress(Mpa)	93.05	118.512	143.015	396.244

D2 Bone

Table 2. Comparison of Magnitude of stresses (Mpa) recorded at different angulations of angulated abutments under axial loading of 178N in D3 density bone

	Zero	10deg	20deg	30deg
Overall stress(Mpa)	94.4093	122.477	148.723	395.997

D3 Bone

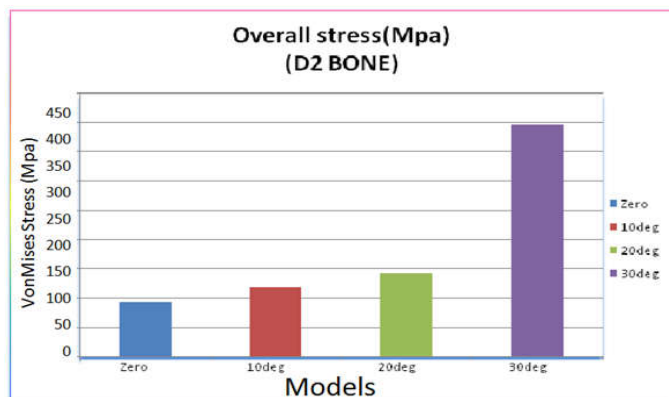


## RESULTS

### I) Magnitude of stresses in d2 density bone

A) Order of the magnitude of OVERALL STRESS in axial loading:

$30^{\circ}$  Abutment >  $20^{\circ}$  Abutment >  $10^{\circ}$  Abutment >  $0^{\circ}$  Abutment  
On Axial Loading (178 N) as shown in Fig. 4a,4b,4c and 4d.

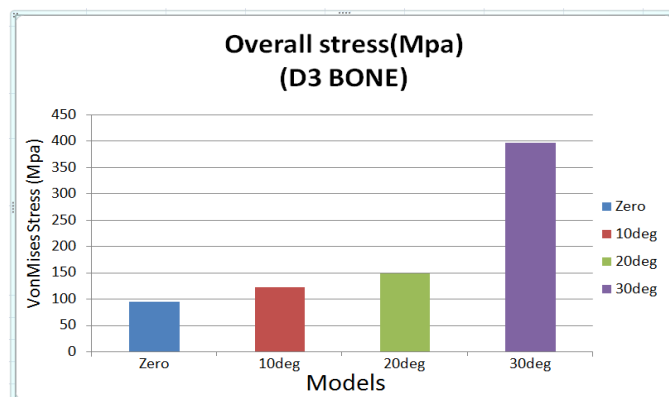


Graph 1. Overall stress of  $0^{\circ}$ ,  $10^{\circ}$ ,  $20^{\circ}$  and  $30^{\circ}$  abutment models in D2 density bone

### II) Magnitude of stresses in d3 density bone

A) Order of the magnitude of OVERALL STRESS in axial loading:

$30^{\circ}$  Abutment >  $20^{\circ}$  Abutment >  $10^{\circ}$  Abutment >  $0^{\circ}$  Abutment  
On Axial Loading (178 N) as shown in Fig 5a,5b,5c and 5d.



Graph 2. Overall stress of  $0^{\circ}$ ,  $10^{\circ}$ ,  $20^{\circ}$  and  $30^{\circ}$  abutment models in D3 density bone

The results showed an increased magnitude of stresses approximately 4.4 folds was observed at overall bone implant interface as the angulations of abutments increased from  $0^{\circ}$  to  $30^{\circ}$  under axial loading in D2 and D3 types of density of bone as shown in Table-1 and Table-2. However no significant differences was observed in magnitude of stresses in both D2 and D3 types of bone.

## DISCUSSION

Stress and strain have been shown to be important parameters for crestal bone maintenance and implant survival. The higher the crestal stress, the higher the risk of crestal bone loss. The

higher the stress factors throughout the implant the greater the risk factor for implant failure (Meijer *et al.*, 1992). Following tooth extraction in the anterior part of maxilla the horizontal bone resorption is almost twice as pronounced as vertical resorption. Lack of bone volume always result in exposure of implant surface, decreased bone-implant interface and finally implant failure. This can be managed either by surgical correction or by positioning the implant in the area with greatest available bone. This is made possible by carefully planned the cases, with use of angled implant abutments. Eger *et al* and Sethi *et al* concluded that angled abutments may considered a suitable restorative option when implants are not placed in ideal axial positions (Arun Kumar *et al.*, 2013). Especially in the maxilla in an esthetic zone an angled abutment allows the placement of implants in the most favorable quantity and quality of available bone in patients with compromised osseous anatomy. In a study, survivability of implants used with angulated abutments ranging from 0-45 degrees, it was observed that the survival function rates of implants with angulated and straight abutments was the same (Sethi *et al.*, 2000). This study was conducted to gain more insight into the influence of different angulated implant abutments on the stress distribution in the alveolar bone surrounding the implant under axial loading.

Xavier *et al.* in his study, he concluded that the model with the straight abutment had slightly higher values of microstrain than the model with the angled abutment (Xavier *et al.*, 2007). Cardelli *et al.* in his study, he reported that bone resorption was recorded at the level of implant neck in close contact with cortical bone. As far as the use of angulated abutment is concerned they concluded that it is necessary to use them and suggested to not exceed the limit of  $25^{\circ}$  (Cardelli *et al.*, 2009). Cavallaro *et al.* and RohitBahuguna *et al.* they both evaluated five abutment divergences ( $0^{\circ}$ ,  $15^{\circ}$ ,  $25^{\circ}$ ,  $30^{\circ}$  and  $35^{\circ}$ ). On the basis of available data in the literature, they concluded that though the compressive and tensile stresses generated through axial and oblique loading increase as the abutment angulation increases yet they are within the tolerance limits of the bone (Cavallaro *et al.*, 2011; Rohit Bahuguna *et al.*, 2013). Arun K *et al.* conducted a study to compare the stress distribution around implant in different bone qualities of D1, D2, D3 and D4 with straight and angled abutments using three dimensional finite element analysis. They concluded that Von mises stress values were increased as the bone quality changes from D1 to D4 (Arun Kumar *et al.*, 2013). In this study the stress distribution around implant in different bone qualities of D2 and D3 with straight and angled abutments was studied using finite element analysis. The anterior teeth were subjected to maximum compressive stress during incising and the force was directed along the long axis of the tooth. In implant with straight abutment the force was directed along the long axis of abutment and implant which results in even distribution of stresses on the buccal and lingual side in D2 and D3 bone qualities. In angled abutments the force would be directed to the area of bone opposite to that of abutment inclination. As the density of the bone increased, the stresses were concentrated on the facial aspect for all the abutments These values are in accordance with the study done by Clelland and Martin D Grass *et al.* (Clelland *et al.*, 1995). Lin *et al.* conducted an analysis of stress on single implants and reported that the cortical bone strain was higher for an angled abutment of 20 degrees than that for straight abutments and bone strain increased as the bone density decreased (Lin *et al.*, 2008). Danza *et al.* studied the stress distribution around a spiral

implant with a 0°, 15° and 25° angulated abutment in D1 and D4 density bones using three dimensional FEA and reported that maximum bone stress was obtained with 15° angulated abutment (Danza *et al.*, 2009). When the stress in the thin (0.5mm) and the thick (1.0 mm) cortical bone due to four different angulated abutments subject to axial loading (178N) were evaluated, it was observed that the overall stress in both the D2 and D3 models with 0°, 10°, 20° and 30° abutments, the  $\Sigma E_{max}$  stress values were 93.05 to 396.24Mpa. However studies state that within a load of 178 N, angulated abutments up to 20° can be placed in the anterior maxilla zone but further clinical scientific evaluation needs to be done. The above reported results of this analysis correlate with findings of other studies that used different investigation methods. Certain limitations of finite element study should be taken into consideration that is geometry of the model was simplified, with a rectangular section. The resultant stress values obtained may not be accurate quantitatively but are generally accepted qualitatively. Chewing forces are dynamic in nature, whereas the study was conducted with static loads. Due to the limitations pertaining to the study, further research regarding three-dimensional finite element analysis combined with long term clinical evaluation has been suggested.

## Conclusion

The following conclusions were drawn from the study

### On axial loading of 178 N

The magnitude of overall stresses were maximum in the 30° abutment compared to those of 0°, 10°, 20° angulated abutments. There was an increased magnitude of stresses of approximately 4.44 folds higher respectively. But, no significant difference in magnitude of stresses was observed in both D2 and D3 density bones.

**Conflicts of Interest:** None

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