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## RESEARCH ARTICLE

### ASSESSING THE PERFORMANCE OF CHECK DAMS TO CONTROL RILL-GULLY EROSION: SMALL CATCHMENT SCALE STUDY

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#### ABSTRACT

Field experimental study was conducted to observe the effectiveness of check dams for reducing runoff and sediment yield in small gully catchment area. In the first phase of experiment, rill-gullies were mapped based on field survey and rill-gully development were measured; and in the second phase, check dams were constructed in particular interval along the gully to assess its effects since 2010. Check-dams in the gully basin have played a very important role in reducing sediment yield by 41.5 percent through trapping sediment and reducing erosion. Check-dams depressed the sediment yield by reducing the power of concentrated flow to remove materials through raising base level of erosion. The sediment deposited upstream of check dams shows distinct sorting. This trapped deposit facilitated the growth of vegetation which again intensifies the stability of deposit and so check dam is proved to be an efficient method of controlling rill-gully in the present study.

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#### INTRODUCTION

Soil erosion is a physical process with significant dissimilarity globally in its sternness and regularity (Poesen *et al.*, 2003; Allen and Welch, 1971). It is indispensable to recognize the interface of the processes leading to the instigation and expansion of rills and gullies for the better management to control maximum utility from land and soil resource for long period (Huang, 2000; Zeng *et al.*, 1995). Earlier workers were designed plot-scale experimental studies to understand the interrelationship between the process involving hydrological, ecological and geomorphological factors (Feng, 2000; Shit *et al.*, 2012a; Shit *et al.*, 2012b; Gray and Leiser, 1982. The factors influence the rate of rill and gully erosion may be considered three headings, namely energy, resistance and protection (Morgan, 2005; Van Liew and Saxton, 1983). Such high sediment yields resulted in unsteadiness in these rill-gully channels. There are several factors that hearten the infiltration of water into the soil and thereby reduce runoff and deceases the erodibility, while any activity that pulverizes the soil, erodability is increases (Fullen and Booth, 2006; Zeng *et al.*, 1999; Fullen and Brandsma 1995).

Lenzi (2002) demonstrated that the check dams constructed by local boulders could be used for gully erosion control and for high-gradient stream stabilization. The major function of check dams is to lessen water velocity and to catch sediments in gullies instead of supplementary soil substance being eroded away (Gray and Leiser 1982; Hui and Mangan, 2000). Although, the provision of check dams is very effective's measure to trap eroded sediments, to stabilize stream channels, to reduce channel slope and to prevent the loss of soil from the gully channel in bad land areas (Singh *et al.*, 2002; Yano, 1968; Zhang *et al.*, 1988).

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Earlier researchers also suggested that the building of check dam systems is one of the most effective measures for the conservation of soil and water in small watershed (Jiang *et al.*, 1994; Xu and Wang, 2000; Xu. *et al.*, 2004).

The usefulness of check dam systems for gully control aids to alleviate the streams and the adjacent land erosion (Xu *et al.*, 2002, Lenzi and Comiti, 2003). In addition to the variations of erosion associated with the frequency and magnitude of single storms, rates of erosion often follow a seasonal pattern. This is best illustrated with reference to a rainfall regime with a wet and dry season (Figure 1). The vegetation growth follows a similar pattern, but peaks erosion was observed later than the rainfall. The most vulnerable time for erosion is the early part of the wet season due to high rainfall; however vegetation has not grown sufficiently to protect the soil (Zokaib *et al.*, 2005; Fang, 1999; Fang 1995; Meng, 1996). Thus, the erosion peak proceeds with the increase of rainfall. Therefore, it is necessary to construct the check dams for trapping sediment and to reduce runoff, and check the soil erosion (Fang *et al.*, 1998; Gee and Bauder 1979; Goel *et al.*, 1996).

In the present study, an experiment was conducted to investigate the effectiveness of check dams to reduce runoff and sediment yield in small gully catchment area of Paschim Medinipur district of West Bengal, India. Here we also analyzed the role of check dams in reducing rill-gully erosion rates and stabilized of gully heads.

#### MATERIALS AND METHODS

##### Study area

The Rangamati gully basin-II, a lateritic upland gully region, extended between 22°24.704' N to 22°24.723' N latitude and 87°17.806' E to 87°17.815' E longitude was selected as the study area (Figure 2).

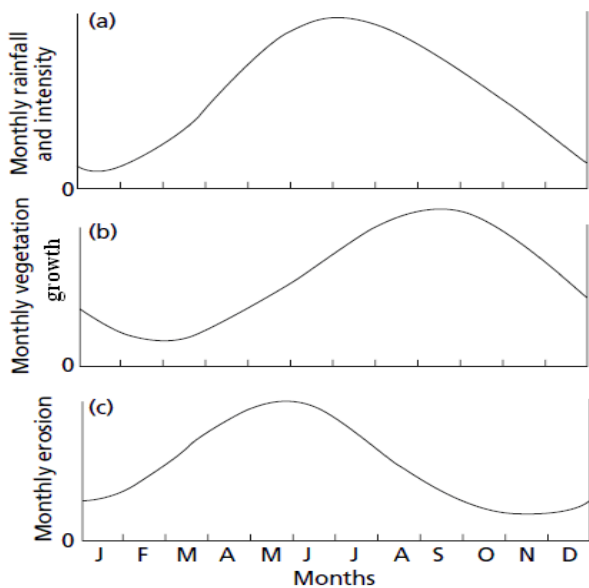


Figure 1. Seasonal cycles of rainfall, vegetation cover and erosion in sub humid monsoonal climate (Krikby, 1980).

The study area is located at the left bank of the Kossi (Kansai) river about the 1 km away from Medinipur town, and covered with an area of 254 m<sup>2</sup>. The region is characterized by tropical monsoon climate with mean annual temperature of around 28.4° C, and the average summer (May) and winter (December) temperatures of 40.9° C and 7.5 ° C respectively. The mean annual rainfall of this region is about 1850 mm. However, the rainfall distribution is irregular, experiencing high-intensity rainstorms during June to September (i.e. > 125 mm h<sup>-1</sup> over short periods), with high erosive potential (the rainfall erosivity factor *R* varies between 1200 and 1500 MJ mm ha<sup>-1</sup> h<sup>-1</sup> year<sup>-1</sup>). The major part of soil profiles has been truncated by hydraulic erosion and underlying horizons (Shit, *et al*, 2008, 2012).

There are important topographic variations within the lateritic upland rill-gully landforms. The average morphometric characteristics of gully basin such as top width, depth and length are respectively about 45 cm, 32 cm, and 6.8 m respectively. The maximum altitudinal difference from the gully top to gully bottom is 7 m. The rill-gully density is 1.72 per m<sup>2</sup>. The average slope of this area ranges between 20% and 30%. The gully basin is covered with primary and secondary succession of vegetation (*Alysicarpus vaginalis*; *Eragrostis tenela*; *Evolvulus alcinoides*; *Evolvulus limunaris*; *Cynodon dactylon*; *Cyperus rotundus*; *Rosmarinus officinales*; *Stipa tenacissima*; *Hedyotis corymbosa*; *Lantana camara*; *Euphoria purpuria*; *Eragrostis cynosuroides*; *Evolvulus nummularia*; *Saccharum munja*; *Panicum maxima*; *Andropogon aciculate* etc.) The gully basin is undulating and vulnerable to soil erosion due to heavy rainfall during monsoon and post-monsoon season.

**Field topographic measurements**

Monitoring of rill erosion in the selected basin was initiated in 2006. Series of check dams were constructed in 2008 (Figure 4). For the assessment of performance of check dam, entire monitoring period (2006-2011) is divided into two phases. In the first phase (Pre-construction phase, *i.e.* initial two years during 2006-2008), rill-gullies were mapped based on field survey and rill-gully development was monitored by erosional pins (bamboo) after rainstorms. The runoff volume, rill-gully lengthening and deepening in basin area were measured regularly.

In May, 2008 twelve porous check dams were constructed at particular interval across the gully with local boulders, pebbles etc. The check dam spacing was calculated using the following method developed by Heede and Mufich (1973). Three check dams were constructed in upper catchment, four dam at middle and five dams at lower catchment were constructed.

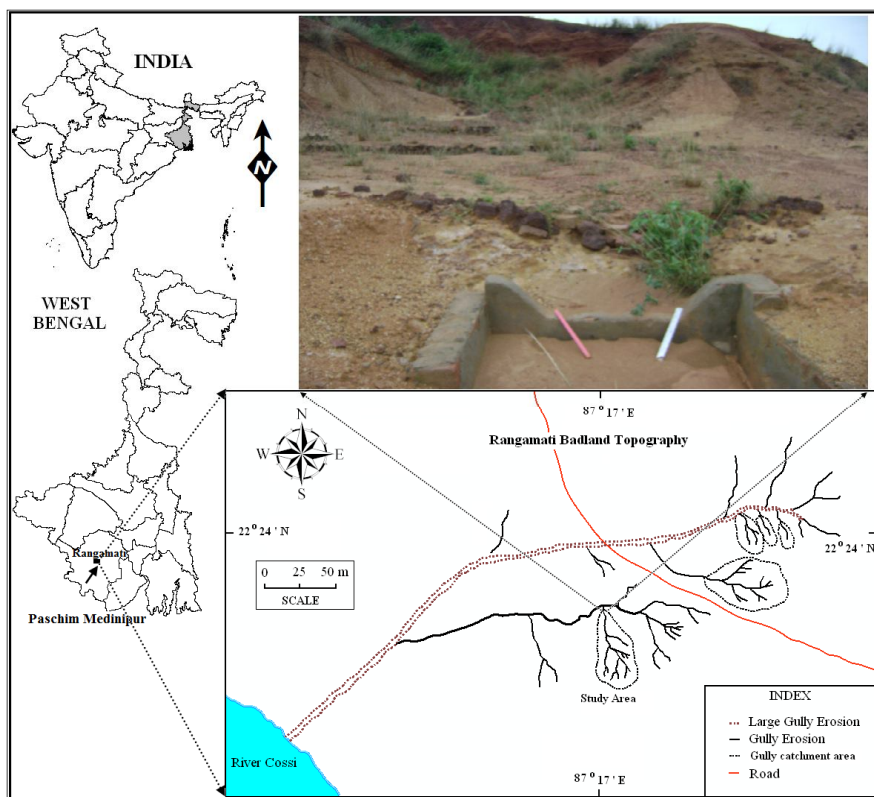
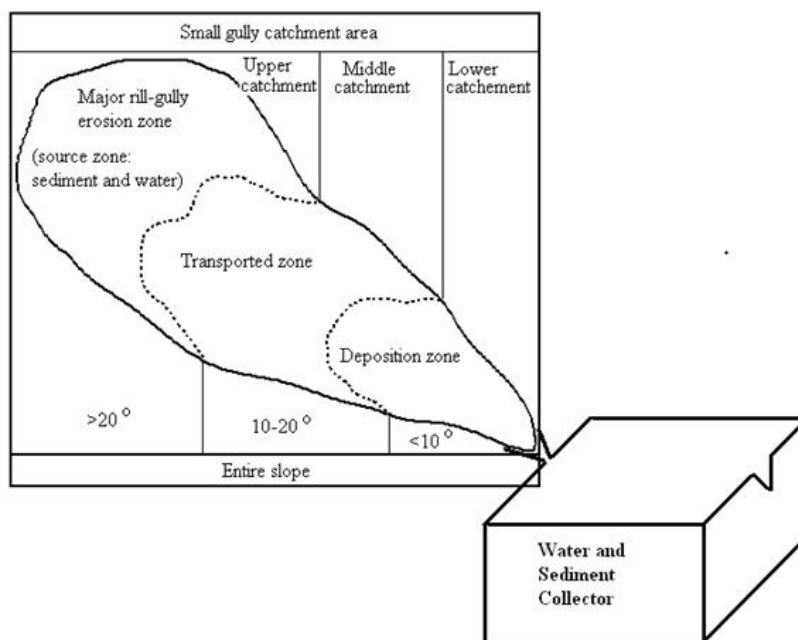


Figure 2. Location of the study area: Rangamati – II small gully basin, Medinipur, West Bengal

**Table 1. Characteristics of check dams at Rangamati Gully Basin-II**

Small gully catchment	Name of the Check dams	Length (m)	Top width (cm)	Height (cm)	Inner slope (Degree)	Repose angle (Degree)	Thickness of the Sediment concentration (cm)			
							Sept, 2009	Oct, 2010	Sept, 2009	Oct, 2010
Lower catchment	1	1	20	40	37	32	12	22	9.6	17.6
	2	6	20	40	40	35	14	19	92.4	125.5
	3	5.5	20	35	38	34	11	20	72.6	132
	4	2.2	20	35	40	30	10	16	24.2	53.24
	5	2.3	20	35	42	38	13	22	54.08	77.28
Middle catchment	6	2.1	20	36	45	46	14	24	49.98	85.68
	7	0.9	20	34	52	40	8	13	11.52	18.72
	8	1.2	20	30	50	45	7	11	11.76	18.48
	9	1	20	30	48	43	8	14	8	14
Upper catchment	10	0.8	20	30	50	42	15	28	15.6	29.12
	11	1	20	30	45	37	7	12	8.4	14.4
	12	1.7	20	30	45	40	6	12	10.2	20.4

Check dams were constructed with rocks, boulder and gravels in the study area. A total of ten check dams were constructed. The length, width, height, inner slope, repose angle of all these check dams are summarized in Table 1. Furthermore, the length of the check dam is varied based on the gully size. The check dams have an effective height between 30 cm and 40 cm and upto 6.0 m long. The inner slope of the check dams is varied from 37 to 52 degree, while the repose angle ranged from 30 – 46 degree.



**Figure 3. Sketch map showing the topography features and erosion process along the small gully catchment**

$$L = \frac{H}{KSoCos\alpha} \dots\dots\dots 1$$

Where, L = Dam spacing along the gully (m)  
 H= Effective dam height (m)  
 So= Original gully slope  
 S= Sediment deposit slope  
 $\alpha = \tan^{-1} So$   
 $K= 1 - S/So$

According to Heede (1976):

$$Spacing = \frac{HE}{K \tan \theta \cos \theta} \dots\dots\dots 2$$

HE is the dam height,  $\theta$  is the slope angle of the gully floor and K is a constant equal to 0.3 for  $\tan \theta \leq 0.2$  and 0.5 for  $\tan \theta > 0.2$ .

The dam height is measured from the crest of the spillway to the gully floor. Check dams were constructed with rocks, boulder and gravels in the study area. A total of ten check dams were constructed. The length, width, height, inner slope, repose angle of all these check dams are summarized in Table 1. Furthermore, the length of the check dam is varied based on the gully size. The check dams have an effective height between 30 cm and 40 cm and extended upto 6.0 m long. The inner slope of the check dams is varied from 37 to 52 degree, while the repose angle ranged from 30 – 46 degree.

**Sediment trapping and Soil properties analysis**

Sediment was collected after each rainfall through partial flume (Figure 3) and the sediment concentration behind each check dam was estimated. Sediment trapped was measured by measuring scale and multiplied by the area for estimating its volume. To study the nature of soil, parameters like soil texture, color of soil, soil consistence, erodability and soil pH, NPK, EC (Electric Conductivity), OC



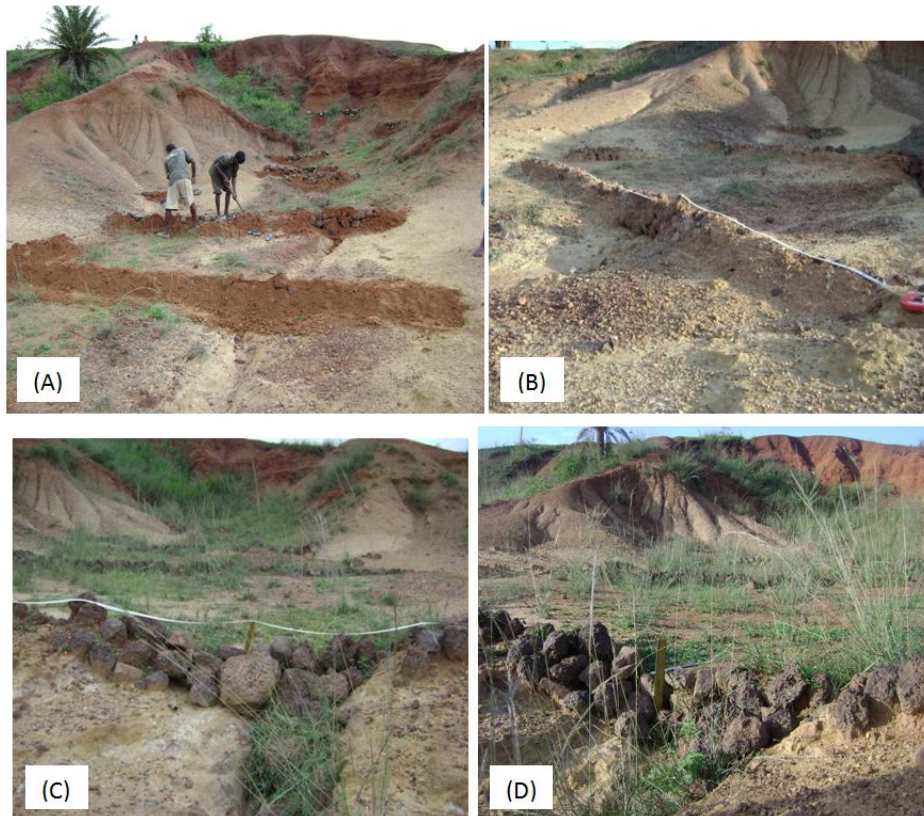


Figure 4. (A) Constructing check dams May, 2008(B) After 9 months constructing check dams, Aug, 2009, (C) After 18<sup>th</sup> months constructing check dams, June, 2010 and (D) After 21<sup>st</sup> months constructing check dams, Sept, 2010

(Organic carbon) were analyzed. Topsoil was collected at 5-10 cm depth from the 3 different places of each check dam. The soil samples were dried through dry oven and from the each site 100g samples were mechanically sieved in the laboratory to sort the sediment into different size groups. The soil texture was determined by the hydrometry method (Gee and Bauder 1979) and the grain size distribution was determined by dry sieve analysis (Geo-chemical Lab, GSI, Eastern Region, Kolkata, and Panskura Agricultural Lab). The performance of the check dams and the effect of their location along the streams in retention of fine sediments were plotted in line diagram. Soil color was analyzed using Munsen color Chart and pH and EC of soil was measured using the digital pH meter and digital EC meter (shit *et al.*, 2010). Soil fertility was also analyzed by NPK and OC using Kjeldahl distillation for Nitrogen (N); Flame photometer for Potassium ( $K_2O$ ) and UV-VIS Spectrophotometer for Phosphorous ( $P_2O_5$ ) respectively. All soil properties were measured after and before constructing check dams.

## RESULTS AND DISCUSSION

### Mechanism of check-dams in retaining sediments and decreasing erosion

At the initial stage of the check-dam, sediments are retained and runoff water is impounded within the check-dam.

At this stage, the check-dam has the function of reducing the erosion in the lower reaches by reducing peak runoff. In the later stage, the flow velocity is reduced due to wider and gentle gradient of the newly formed terraced land. Consequently, sediment transport capacity of the stream is decreased and sediment deposition is observed along the valley of gullies (Figure 4). Meanwhile, grasses grew on the trapped sediment naturally after 18 months of constructing check dams

Table 2 showed the status of deepening, lengthening and widening of valley before and after the check dam construction. For example, during the period from June 2006 to May 2007, the average depth of the valley was 8.89 cm; while after the construction of check dam it is reduced upto 5.67cm. It is also observed that the average rate of valley lengthening was 8.44 cm before the construction of check dam, while it is reduced upto 7.22 cm after the check dam construction. The result also revealed that the average width of the valleys was 10.50cm before the check dam construction, whereas, it is decreased upto 8.00cm after the check dam construction (Table 2, Figure 4). However, the valley length, width and depth were relatively high before the construction of check dams and it is reduced after the construction of check dams due to partial filling with trapped sediment (Allen and Welch, 1971).

Table 2. Erosion Measurement during monitoring periods (2006-2010)

Monitoring Periods	(Before check dams)						(After check dams)					
	June, 2006 – May, 2007			June, 2007– May, 2008			June, 2008 – May, 2009			June, 2009– May, 2010		
	VD	VL	VW	VD	VL	VW	VD	VL	VW	VD	VL	VW
Rills or gullies erosion	VD	VL	VW	VD	VL	VW	VD	VL	VW	VD	VL	VW
Min (cm)	4	5	6	6	7	7	3	4	6	3	4	3
Max (cm)	15	12	16	21	14	15	9	10	10	8	13	9
Mean (cm)	8.89	8.44	10.5	9.88	9.78	11.11	5.67	7.22	8	5.56	7.78	5.33
SE (cm)	1.31	0.76	1.06	1.71	0.87	1.06	0.67	0.68	0.41	0.60	0.91	0.62
SD (cm)	3.95	2.29	3.21	5.13	2.63	3.18	2.00	2.04	1.22	1.81	2.73	1.87
N	35	28	30	35	28	30	35	28	30	35	28	30

VD= Valley deepening; VL= Valley lengthening; VW= Valley widening

### Sediment trapping by Check dams

For each check dam, sediment concentrations were measured (Table 1). The thickness of sediment concentration behind each check dam varied from 11 to 28cm. Moreover, the result of the analysis showed that the length of the depositional surface behind each check dam was positively related to the height of the check dam and the gradient of the depositional surface ( $r = 0.4s2$ ), but negatively related to the original channel gradient. The volume of sediment is trapped by the check dams ranges from 8.0 to 92.4 m<sup>3</sup> (mean±standard deviation 30.70±29.16) upto September, 2009; whereas, in October, 2009 the sediment concentration in ranged from 14.0 to 132.0 m<sup>3</sup> (mean±standard deviation 50.54±44.05) (Table 1 and Figure 5). The result of the study also showed that is strongly correlated with the length of the gully ( $r = 0.93$ ;  $p < 0.0001$ ). Moreover, the height of the check dams were positively correlated with the sediment volume,  $r = 0.61$  in September, 2009 and  $r = 0.58$  in October, 2009. Negative correlation was found between inner slope angle and volume of sediment concentration in September, 2009 ( $r = -0.53$ ) and in October, 2009 ( $r = -0.57$ ). Additionally, repose angle also demonstrated weak negative relationship with the sediment volume in September, 2009 ( $r = -0.23$ ) and in October, 2009 ( $r = -0.27$ ).

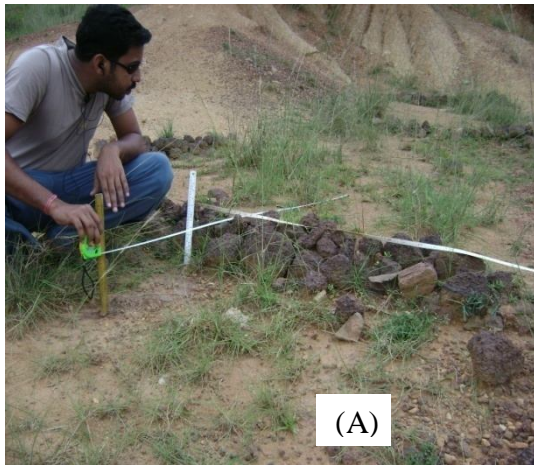


Figure 5. Typical porous check dams constructed with local bolder for sediment trapping and reducing runoff. (A) Sept, 2009, and (B) Oct, 2010

### Comparative assessment of soil loss and runoff volume

A comparative assessment is carried out to estimate the role of check dam in soil detachment and runoff volume. Runoff volume drastically reduced after the construction of check dam. The same is true for sediment discharge (Figure 6).

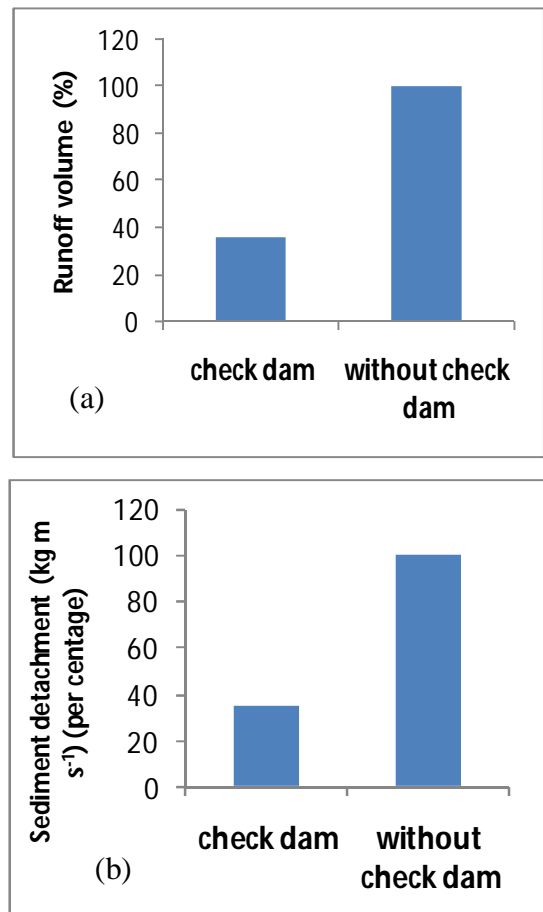


Figure 6. Effect of check dams (a) Estimation of runoff volume in relation to check dams (b) Estimation of soil loss in relation to check dams

### Check dams and terrace formation

In the reach upstream of each check dam, the degree of stream channel deformation was monitored by longitudinal profiles (Figure 7). The longitudinal profiles showed the deposition of sediments after the check dam that leads to develop terrace in the channel. The terrace with relative altitude up to 28 cm equivalent check dam height was formed in the gully. The detached sediment forms the upper sediment source zone start moving downstream. Being obstructed by the check dams velocity as well as carrying capacity of the runoff reduces that leads to sedimentation at upstream of each check dam. This sedimentation partially fills the channel that developed horizontal surface (terrace), where runoff loses its velocity and transport power (Figure 7). This further reduces carrying capacity and helps in further siltation. The result is also corroborated with earlier research work conducted by Van *et al.*, (1983).

### Soil particles analysis

Physical properties were also measured of the deposited material behind each check dam. The allocation of grain size of the sediments dropped behind the check dams depends on the available energy and efficiency of check dam to reduce velocity and transporting power. However, the analysis has been performed in the upper (>20 degree slope), middle (10 to 20 degree slope) and lower (<10 degree slope gradient) catchment area separately (Table 3). The result of the analysis showed that percent of sand particles were maximum in all the catchment areas in comparison to the silt and clay particles. Moreover, deposition of silt percent is more or less same in the upper and middle catchment area; while the deposition of clay percent is maximum in the lower catchment area (Figure 8). It is due to construction of check dams, water cannot pass through the dam easily,

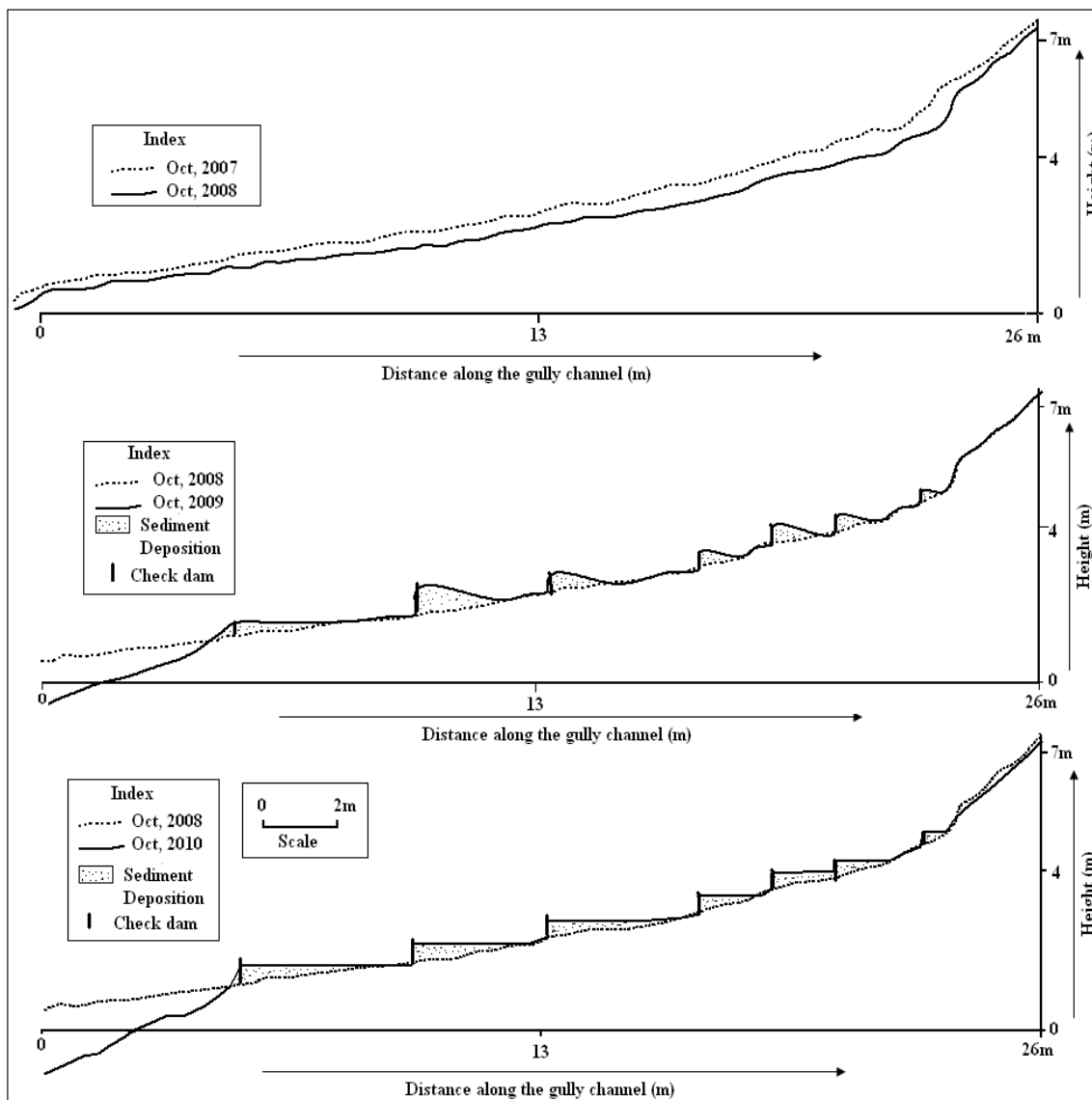


Figure 7. Terrace formations due to check dams trapping the transported soil

so most sediments are trapped, and consequently, a backwater condition was developed that reduces the flow velocity. Additionally, the deposited material intimately resembled the coarse bed load existing in the unique channel and infatuated the distinctive particle size allocation.

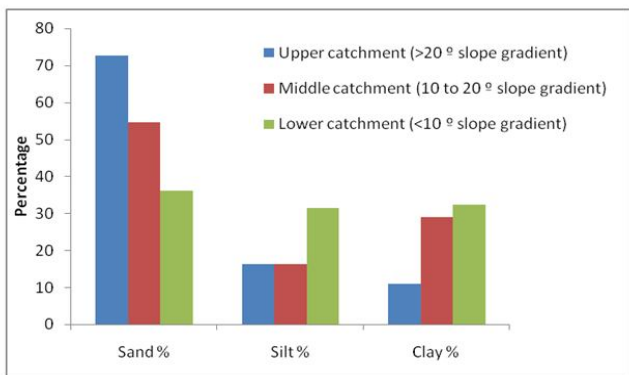


Figure 8. Represent the sand, silt and clay percentage trapped by check dams

The depositional surfaces at the back of each check dam can be divided into different soil textures, according to the maximum diameter of the bed load particles (Figure 9). The upper part mainly consists of sandy loam, middle catchment with sandy clay loam and the lower catchment area consists of clay loam. This means that the check dam at the far downstream section performs much better in trapping fine sediments compared to the check dams located in the upper and middle sections of the streams. However, the result is also corroborated with the recent study (Hassanli *et al.*, 2009).

Furthermore, to appraise the effect of porous check dam position in a gully for the trapping of fine sediments, the grain size allocation of the sediments trapped by the check dams located at the far upper catchment section, at the middle section and at the far lower catchment section of each studied gully were also compared. In porous check dam, fine sediments were passed through the check dam by water flowing downstream. Figure 9 shows the particle size distribution curves corresponding to the three check dams located in Rangamati-II gully basin. The results also illustrated that the fine sediments were trapped far from the check dams in comparison to the middle and upstream sections. This significant difference could be due to the location of the check dam and the effect of intensive vegetation covers in the downstream reaches. The results of the study are also ratified with the previous study (Hassanli *et al.*, 2009; Shafahi Bajestani 1994; Gee and Bauder, 1979).



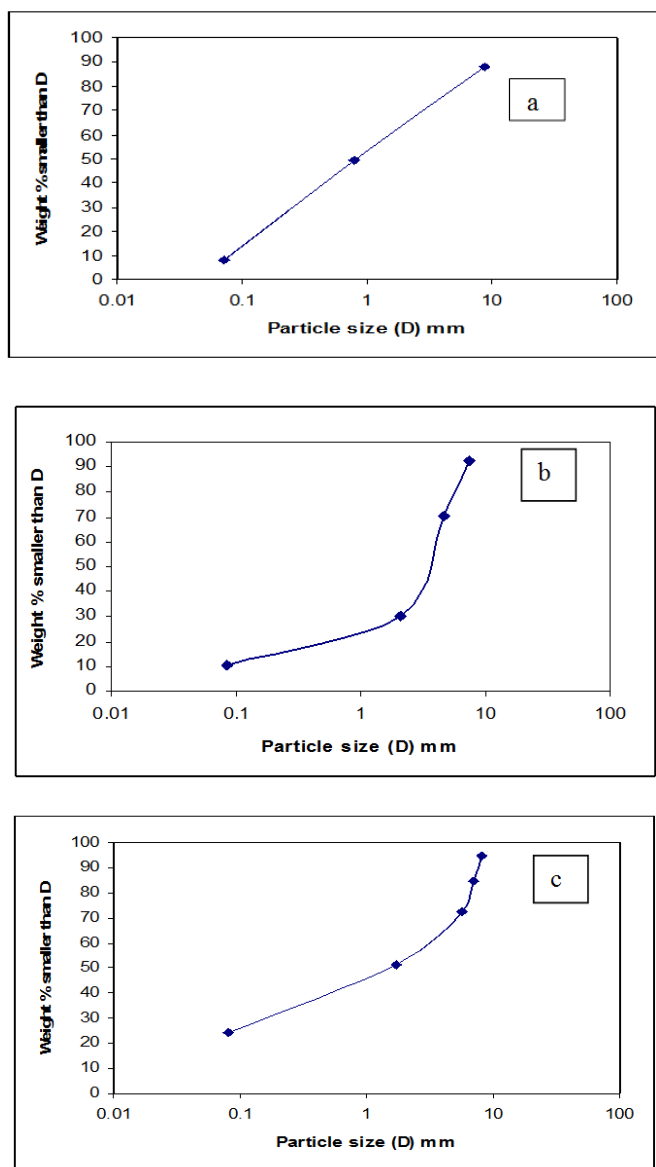


Figure 9. Represent the particle size distribution of trapped sediment (a) Upper catchment (>20 ° slope gradient), (b) Middle catchment (10 to 20 ° slope gradient), and (c) Lower catchment (<10 ° slope gradient)

**Check-dams and the soil fertility**

Another important aspect of check dam construction is to increase of soil fertility in the neighbour region. To estimate the soil fertility, nitrogen (N), phosphorous (P), potassium (K), OC, soil pH, and EC were measured before and after the check dam construction. The result of the analysis showed that soil nutrients were dramatically increased after the check dam construction (Table 4). Furthermore, the results also demonstrated that the acidity of soil is reduced after the check dam construction. However, these may aid to grow the vegetation in nearby region of check dams and further reduce the soil loss.

**Conclusion**

Results from this study suggested that the installation of check dams produced positive effects in reinforcing upstream channel stability. In the reaches upstream of each check dam, the stream channel became wider and flatter. In addition, the depositional surface behind the check dams was relatively stable when the storage capacity was filled. Hence, the check dams mechanism can provide as efficient energy-absorbing dissipaters, then channel erosion can be abridged and it can be anticipated that the stream channel is to be steady in the long-term (Liu, 1983 Liu and Lin 1984). Check-dams in the study area have played an extremely imperative role in dropping sediment yield by trapping sediment and minimizing the frequency and intensity of soil loss. Furthermore, in case of sediment trapping, check-dams lowered the sediment yield by reducing the frequency and intensity of hyper-concentration flows and by reducing soil erosion in gullies through raising their erosion base level. To attain a high preservation of fine sediments it is suggested that porous check dams are assembled towards the lower catchment sections rather than in upper catchment sections. And, the construction of check dams in the study area may also aid to increase the soil fertility that helps to grow the vegetation in the nearby region ( Fullen and Booth, 2006). However, the present work is highly relevant in the context of degradation of land resource and to increase productivity by retaining as well as increasing quality of land. There is increasing awareness of the need to protect our natural environment in order to meet present and future requirements. In this circumstance, the intensive study on the mechanism of rill-gully erosion with spatio-temporal variation is necessary for remedial measures of rills and gullies erosion. The function of check-dams in soil conservation measures should be remunerated ample concentration in the future. It is essential to fortify construction and management of check-dams for preserving and even promoting their sediment trapping capacity and reducing the frequency of high sediment yield.

Table 3. Texture of the trapped sediments corresponding to the check dams

Location of the Check dams	Number of check dams study	Sand %	Silt %	Clay %	Soil texture
Upper catchment (>20 degree slope gradient)	3	72.68	16.32	11.00	Sandy loam
Middle catchment (10 to 20 degree slope)	4	54.64	16.30	29.00	Sand clay loam
Lower catchment (<10 degree slope)	5	36.20	31.42	32.38	Clay loam

Table 4. Soil properties of gully floor after and before constructing check dams in gully basin area

Soil Properties	Catchment area	Color	Consistence	Erodibility	NKg/ hect	PKg/ hect	K Kg/ hect	OC (%)	pH	EC (Mili mho/cm)
Before Check dams	Upper catchment	Grey-brown	Slightly friable	High	710	116	21.9	0.69	5.16	0.063
	Middle catchment	Grey	Stickly	Moderate	728	83	5.6	0.78	4.79	0.027
	Lower catchment	White- grey	friable	Moderate	746	89	7.4	0.74	4.80	0.032
After Check dams	Upper catchment	Grey-brown	Slightly friable	Moderate	876	86	6.4	0.87	4.64	0.023
	Middle catchment	Grey	Stickly	Slight	842	98	3.9	0.83	5.47	0.035
	Lower catchment	White- grey	Plastic	Slight	965	93	8.9	0.93	5.21	0.022

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